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BOX PATENT APPLICATION
Assistant Commissioner for Patents
Washington, D.C. 20231

Re: Application of Harry B. SMITH
METHOD AND MEANS FOR INCREASING INHERENT CHANNEL
CAPACITY FOR WIRED NETWORK
Our Ref. A7583

Dear Sir:

Attached hereto is the application identified above including 33 sheets of the specification, claims, and 14 sheets of informal drawings. The executed Declaration and Power of Attorney, Assignment and the Small Entity Declaration will be submitted at a later date.

There is no claim to priority.

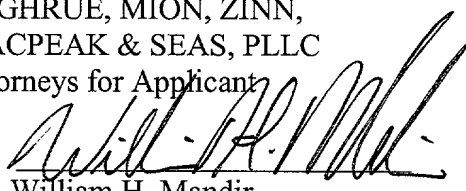
The Government filing fee is calculated as follows:

Total claims	27 - 20	=	7	x	\$18.00	=	\$126.00
Independent claims	6 - 3	=	3	x	\$78.00	=	\$234.00
Base Fee							\$690.00

TOTAL FEE	\$1050.00
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Please charge the filing fee of \$1050.00 to Deposit Account No. 19-4880. You are also directed and authorized to charge or credit any difference or overpayment to Deposit Account No. 19-4880. The Commissioner is hereby authorized to charge any fees under 37 C.F.R. §§ 1.16 and 1.17 and any petitions for extension of time under 37 C.F.R. § 1.136 which may be required during the entire pendency of the application to Deposit Account No. 19-4880. A duplicate copy of this transmittal letter is attached.

Respectfully submitted,
SUGHRUE, MION, ZINN,
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METHOD AND MEANS FOR INCREASING INHERENT CHANNEL CAPACITY FOR WIRED NETWORK

CROSS REFERENCE TO RELATED APPLICATIONS

5 This application is filed under 35 U.S.C. § 111(a), claiming benefit pursuant to 35 U.S.C. § 119(e)(1) of the filing date of the Provisional Application 60/154,781 filed on September 20, 1999 pursuant to 35 U.S.C. § 111(b). The Provisional Application is incorporated herein by reference for all it discloses.

BACKGROUND OF INVENTION

10 This invention relates to a unique receiver system which improves the Signal-to-Noise ratio capability of receiving signals, compared to conventional receiver practices, and by processing stored received data in near-real time, reduces the inherent affect of thermal noise. This dramatic improvement in the performance affords greater flexibility with respect to several relevant parameters, such as for example, bandwidth, access time, and multiplex ability and accordingly is beneficial in a wide range of commercial and military markets. The invention is applicable to a variety of wireline telecommunications media and data applications including the "Internet".

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20 There are few communication systems that cannot benefit from a significant reduction in the inherent thermal noise that results from necessary amplification. Previous efforts have been expended to conceive, improve and develop a "wireless" antenna and receiving system that has a dramatically improved signal-to-noise ratio and related characteristics. In this process extensive software programs were conceived and

developed for both simulation and solution-to-problem purposes. These techniques have been adapted to wired communication. The result includes means for greatly improving the signal-to-noise ratio that can be obtained from a sequence of digitally converted received signals that are stored and then processed in a wired system suited to the
5 "INTERNET".

The description herein describes the signal-to-noise improvements and involves both "hardware" and "software". These unique features provide the potential for increasing channel capacity and other performance improvements. These opportunities for improvement occur at several links in the operation such as with the service
10 provider(s) and at various "gateways" that receive the communicated modulated signal.

Processing is achieved using modern integrated circuits in an off-line manner that does not adversely compromise the bandwidth of the system. The time for such processing results in a "transport" time delay, which can be made tolerable. The resulting "near real time" performance provides the potential to obtain dramatic S/N improvements
15 beyond that predicted by classic analog developed theory.

Thermal noise is introduced as a result of necessary amplification in the reception of a signal; such noises are usually a limiting factor in the ability to identify a "weak" signal. If such noise is substantially reduced, there results a potential for improving the receptivity of the signal, thereby also allowing for tradeoffs in parameters such as
20 bandwidth and optimization of multiplexing abilities. When transferring packets of digital data, as used in transmitting Internet information, the noise affects the reading in that detecting each "plus" digit so as to be able to distinguish it from the absence of signal which constitutes a "minus" digit. As noise is reduced, weaker digits can be read

more reliably and a lower “error rate” results. For a given “acceptable error rate”, the improvement in signal-to-noise can be used to increase the number of signals that can be multiplexed and maintain the same error rate and thereby increase the system capacity.

The unique techniques used in the processing are intended to be performed
5 digitally to obtain the desired precision and preserve the numerical accuracy. It is consistent with such processing to convert both the signal and the noise introduced at reception to a digital format. Thus, despite the fact that the packets are already digital, it is more consistent to restore the signal to analog and then convert the analog signal plus noise to digital signal-plus-noise. This, in some respects may be unnecessary because the
10 digital packet that is corrupted by the analog receiver noise probably will reduce to the same digital numbers as the more pedantic approach of converting to all analog and then conversion back to digital. These options are discussed later in connection with block diagrams (Figure 1 and Figure 3).

The ability to reduce thermal noise limitations that are inherent in any receiving
15 system, beyond the results obtained by averaging several trials, is unique. Such achievement is facilitated by the digital nature of the process (specifically the “storage” of the digitized numbers). However, “being digital” does not in itself produce S/N improvement. Rather, it is the subsequent use of unique iterative processing using an inherent storage and a matrix that serves as a “change sensor” that has unique properties
20 herein described that causes each step to act as a part of a converging iterative procedure with logic that applies to each of the several iterations.

The improvement over merely averaging the noise is the result of improving the “entropy” of the overall process. The processing steps bring a degree of order not

initially present. Such order is the result of forcing each and every sample of the noise in a special numerical array to change polarity in a carefully defined manner. This occurs during successive trials, each of which serves as a row of the stored matrix. From this stored information, inherent in the digital matrix, a unique iterative processor, to be
5 described later, will extract the desire information by off-line processing using the signal plus noise flow shown in Figures 9 and 10.

SUMMARY OF THE INVENTION

10 It is, therefore, an object of the present invention to provide an improved receive system that provides the ability to distinguish between signals with low power levels thereby substantially increasing the S/N ratio of the system.

A further object of the present invention is to provide a digital processing method, which can be carried out in software and which uses a specially conceived integration of circuit hardware.

15 A further object of the present invention is to provide a receive system whereby received signals are sampled periodically and the noise component of the overall received signal sample is estimated from each received signal plus noise sample, leaving nearly noiseless samples of the received signal.

20 A further object of the present invention is to provide a method for near-real-time iterative processing, which is performed offline with respect to stored data using a number of iterative steps.

A further object of the present invention is to provide “polarity change” sensing means, referred to herein as a Topographical Change Sensor (TCS), appropriate for executing the several steps of the noise reducing iterative process.

A further object of the present invention is to provide an iterative sequence
5 programmer that provides, in “near real-time,” an appropriate control of value steps, and responses to changes sensed by the TCS.

To achieve the above and other objects of the present invention the following
embodiments are provided as examples for the invention. Persons skilled in the art
would be aware of techniques available to modify various elements of the invention
10 without straying from the scope and spirit of the invention.

The received signals are amplified and presented to Analog-to-Digital (A/D)
converters where digital representations of IN-phase (I) and Quadrature (Q) components
of the received signal can be determined. Incidentally, it is in the amplification stage that
most of the noise, which comprises the overall system noise, is inherently introduced, as
15 in most receive systems. A phase reference can be established for subsequent processing
and the I component, also known as the I-vector can be set to this phase reference while
the Q component, or Q-vector can be established 90 degrees out of phase with respect to
the reference.

A clock reference for the A/D conversion is synchronized with the phase
20 reference. Each of the I and Q components, thus, contains both signal and noise and may
include other unwanted signal as well, in the form of “cross talk”.

Further, a multi-step process is performed on the collected data wherein a matrix
for each of the I data, as well as the Q data, samples is initially created which includes

several samples of signal-plus-noise data. The data is formatted and applied to an iterative process scheme consisting of an "iterative sequence programmer" and a special topographical number array that serves as a "change sensor". Upon completion of the iterative processing, "noise-only" data results, which is the net algebraic sum of the different iterative values. The noise-only data is subtracted from the stored signal-plus-noise samples leaving the signal, with the noise greatly reduced.

The invention thereby provides an improvement to the entropy of a sequence of events that have previously occurred and have been stored.

BRIEF DESCRIPTION OF THE DRAWINGS

The objects and feature of the present invention will become more readily apparent from the following detailed descriptions of the preferred embodiments taken in conjunction with the accompanying drawings in which:

FIG. 1 shows typical roles of the invention at different places in the overall information transfer system where the potential improvement is substantial.

FIG. 2 illustrates an overall signal enhancing system configuration of the system in accordance with a preferred embodiment of the present invention. This block diagram shows an iterative processing scheme including a Topographical Number Array, which is transformed into a Topographical Change Sensor (TCS) in accordance with an embodiment of the invention.

FIG. 3 illustrates various means of connecting to the signal as provided by the transfer network shown in Fig 1.

FIG. 4 (a) and (b) is a computer printout illustration of a method of forcing the noise samples to transition through zero at appropriate points in the number array.

FIG. 5 (a) and (b) illustrates a method of inputting preprogrammed voltages in “Regular” and “Reverse” manners in accordance with the present invention.

FIG. 6 (a) and (b) are computer simulation printouts illustrating left and right topological groupings of signals plus noise in accordance with the present invention.

FIG. 7 is a combined computer printout similar to Figure 4 above showing the effects of column shifting to place this configuration in equilibrium so as to serve a change sensor.

FIG. 8 is a Table of Initial conditions and instructions that help establish the initial or “zero iteration” used in the process described by the Figures that follow.

FIG. 9 is a logic tree that illustrates how the results from FIG. 7 and 8 are utilized to select a next iterative probe value.

FIG. 10 is a flow diagram that shows how the results from Figure 9 are used to control the iterative process so as to make it converge and provide a very accurate estimate of the noise for each trial.

FIG 11 illustrates how additional “augmented” logic is coupled to Figure 9 using information from the history of two or more results from later iterations.

FIG. 12 is a printout indicating the type of numerical results from the above series of operations.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

Several aspects of the present invention are specifically directed to improving the signal-to-noise of a received signal-beyond what would be predicted by classical information theory. These aspects are important to distinguish. Foremost of these aspects is the “offline” processing of stored information. Storage occurs as analog-to-digital conversion is performed resulting in a series of digital representations of the received data.

Subsequent processing is achieved using modern integrated circuits in an “offline” way that does not adversely affect the bandwidth of the system. Offline processing results in a tolerable transport time delay and as a consequence of the delay, “near real-time” performance results. It is this aspect that presents fundamental opportunities over what can be accomplished in conventional real-time processing. Departure from real-time accounts for a potential to obtain signal-to-noise improvement substantially beyond that achieved by merely averaging noise samples and applying the average to a matched filter. If one were to attempt to attribute the improvement over simple summing, it would lie in the improvement of the entropy of the overall process. The present invention has brought a degree of “order” not previously present.

The order achieved by the present invention is the result of iteratively forcing each and every sample of the noise to change polarity in a carefully defined manner, which is one of the primary aspects of the present invention. The ability to reduce “thermal-noise” affects, inherent in any receiving system, to a level below that which can be achieved by the averaging of several trials is unique. This achievement is facilitated by the “digital” nature of the process. However, the “digital” nature itself does not

produce the achievement. Rather, it is the subsequent use of the digital data in the special iterative process that accomplishes the goal.

The invention, basically, consists of an improvement to the entropy of a sequence of events that have previously occurred and have been stored.

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THEORY OF OPERATION

The theory of how the “matrix” configuration and its related “iterative process” can determine the “noise value” of each and every trial will be described after a brief introduction about the characteristics of the overall method.

10 The conceptual basis of the overall method is an example of the use of numerical logic, (in addition to simple relationship equations) to quantify functions. Such a method is based on examinations in terms of confirmations and contradictions that result from numerical actions. The reduction-to-practice of such a method lends itself to the use of multiple integrated “circuits on a chip” that consists of additions and subtractions. Each
15 step provides a known, yet different numerical impact. The resulting range of consequences is explored by a closed loop iterative processor, which is used to obtain a noise estimate of each sample from each trial. The sensing for such feedback loops requires two inputs name by the average and the input nearest to the average. The sense consequences in near-real time provides the means for overcoming the conventional
20 perceived notion that reduction of noise cannot be extended beyond that which is achieved by simply averaging trials. With the approach, to be described, the noise contribution from each trial can be reduced to values arbitrarily close to zero.

The block diagram of Figure 2 will further explain these operations and resulting consequences.

If the input signal (plus noise) is in analog form, an analog-to-digital converter produces a digital representation at an appropriate rate to accommodate signal modulation. The rate is controlled by a local timing clock that samples the incoming signal plus associated “thermal” noise that results primarily from the signal amplification.

5 Each such digital signal or “trial” is injected with i.e. added to, many different predetermined digital values that differ from each other by small increments that are contiguous and encompass virtually the entire minus (m) and plus (n) value range that is probable. These successive and contiguous sums can be considered as (m + n) columns of a matrix with successive trials forming the different rows.

10 Typically, two successive trials and the average of these trials form a “two by (n+m) + 1) matrix”. Here “n” represents the number of columns injected with minus values, while “n” is the number injected with plus values and the “1” represents the column of zero injection. Typically n+m+1 might be about 41, or more, to yield a 2x41 matrix. A “third” row might be used under some circumstances, as well.

15 As a result of the above process the noise component of each signal plus noise sample for each trial will transition from plus-to-minus or minus-to-plus and therefore go “through zero” in a unique column. This is illustrated by Figure 4(a) and 4(b). These figures show both the “m” values Fig. 4(a) and the “n” values Fig. 4(b). The first column of Figure 4(b) is the “middle/center” column of a combined left and right Figure 4. The information is shown separately in a right portion, Figure 4(a), and left portion, Fig. 4(b), simply to enhance the readability of the entries. The “zero” or “near-zero” values are circled. Sometimes two adjacent plus and minus columns encompass the zero value and in this case both columns are circled. It must be remembered that Figure 4(a) and 4(b)

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are not available in a noise only form and the matrix is constructed by the use of the noise samples in the simulation. They are used here simply to provide an illustration of why the numerical number matrix works. It should be apparent that when the signal-plus-noise is included, as in the entries shown in Figure 6a and 6b, the places where the noise passes through zero will make the entry at these corresponding places, at the “average” and for each of the trials, consist of the signal value, although the identity of such columns are not known until after the iterative process is performed.

The next functional task is to identify for each trial and the average row of the matrix pertinent columns that will become involved in an “iterative” process of several iterations or steps. Each such iteration is a “closed loop process” in which the matrix becomes a “change sensor”. Also as part of this process a series of iterative probes each of known magnitude and “polarity” are used to control the next step of the processing using consequences from the previous step.

The matrix which can be considered a “topological number array” is shown in Fig. 6 (a) and (b) and is transformed into a “change sensor” (or detector) by placing the column entries of the two (or more) rows into equilibrium about the zero column which is the topocentric point of the of number array (or matrix). This is accomplished by determining the deviation between the average and the two individual trials. This scalar quantity is independent of the signal and is simply the signal plus noise of each trial minus the signal plus noise average. This can be designated as IA (or QA) where the A indicates that it contains no signal because the signal cancels in the digital plus noise minus the digital plus average noise calculation. IA is simply the deviation value and is known, for the two trial cases the value is plus and minus equal magnitudes. For the

“other than average row” this amount of deviation is translated into an equivalent column shift which is simply the magnitude divided by the column spacing to yield an approximate number of column displacements with the polarity of the deviation determining whether the column shift is to the left or to the right.

5 The preceding measures have partially endowed the topological number array with sensor capabilities; it is necessary in order to complete the task to provide an “error sense” to its ability to make discrete (i.e. “sharp”) comparisons. Such needed capability is provided by reversing the plus-to-minus formatting of the numbers in one of the rows; the “average” row is selected for this role. Thus instead of preprogramming the
10 contiguous injection number from minus to plus those values are injected in a plus-to-minus fashion, i.e., in reverse order. This provides a bipolar detection or sensing capability.

Figure 7 shows the topological array, which is the “Equilibrium State”, and with the “regular” and reversed inputted numbers as shown in Figure 6 (a) and (b).

15 This is a qualified change detector to accommodate each iterative probe. The necessary response, however, requires the logic provided by the Fig. (9) so that the appropriate iterative steps are used in the process shown in Figure 10 (and 11) which provide the desired noise estimate for each overall trial when added algebraically.

20 The iterative process is performed at a slower rate than that for the A/D sampling rate. This is accomplished by using a sub-multiple of the basic clock rate and is shown in Figure 2 as the “divide by 3”. (This number can be selected as appropriate for each application.) The slower rate requires the storage of the basic samples (the information in the iterative matrix is inherently stored by its nature.) The iterative process can be

conducted at a slower rate because the off-line nature of its implementation does not affect the bandwidth handling capability of the system.

Each noise estimate can be cancelled from the signal-plus-noise value of each trial as shown in Figure 2. This cancellation involves the delay (and storage) of the signal-plus-noise as shown in Figure 2 so that noise estimates from like trials can be correlated.

DETAILED DESCRIPTION OF OPERATION

Various methods of connecting to the “wirelines” are illustrated by Figure 3 (a) (b) and (c). The most straightforward to understand is shown in (a) which is simply the use of two wires to obtain two inputs with the “same signal” (with different noise values introduced at each input). This constitutes two trials with like signals and different noise. As such other amplification and analog to digital conversion results in two signal plus noise column sequences that can be used as two rows of a topological number array or matrix. The process as described previously is applied and will be described in more detail by reference to Figures 9 and 10, as follows.

Since this type of connection uses twice as many wire connections, the channel capacity of the network is reduced by a factor of two. Also there is no assurance that the two “signals” will be equal as assumed for illustration. Thus this method is used only to illustrate the “two wire” method; and the other options are resorted to.

The first alternative is to use a single connection and receive two (or more) signal plus noise samples in sequence. This necessitates doubling the sampling rate with a resulting penalty. However, the processing methods remain the same with the two signal-plus-noise samples being used sequentially. This calls for a sampling rate twice

as fast as the optimum Nyquist criteria for a modulated signal and results in a sacrifice of 3 dB. However, the tradeoff for near complete cancellation of noise for each successive pair of samples (trials) is significant particularly when considering that the higher noise values are identified and virtually eliminated. This small sacrifice for a potential improvement of 30 dB, or more, net improvement is a worthwhile tradeoff.

A more optimum approach, illustrated in Fig. 3(c), involves the use of in-phase and quadrature components as the two signal-plus-noise samples used for forming the topological number array or matrix. This involves sampling the signal (plus-noise) at two phases separated a net of 90 degrees apart; this can be accomplished by a 90°-phase shifter (or an equivalent plus 45 and minus 45 phase shift in the two lines). A more elegant mechanization is to perform this shift as part of the analog-to-digital process by sampling the analog-to-digital converter of the two signals the equivalent to 90 degrees apart. The mechanization is similar but this approach requires processing both the “In phase and quadrature channels separately. Also the subtraction of the estimated signal from the actual signal is a vector subtraction that takes place at a 45 degree reference.

As mentioned previously as part of the Theory of Operation the first numerical action consists of deliberately changing the polarity of the noise portion of the signal-plus-noise voltage of each and every trial. This forced change is accomplished by providing a series of contiguous voltage increments that span a range of about minus one volt (-1.0) to plus one volt (+1.0) in increments on the order of .05 volts or less, thereby forcing the change of polarity to occur in one column, or an adjacent pair of columns. There is much flexibility in the number of voltage increments and the “graduation” of their spacing. As each “trial” of signal plus noise is entered into this series of columns, a

network of trials, or matrix, is formed which is referred to as a topographical number array or matrix. The addition of the value inserted into each column creates a “new noise” for each column. As a consequence of these additions, there results one column in which the net polarity of the noise-only portion changes (because the voltage in that column is opposite to that of the noise). While this is focused usually in a specific column, this condition can occur between adjacent columns giving rise to interpolation between adjacent columns.

A series of trials, each consisting of independent samples of signal-to-noise was used in simulation. It corresponds to each digital value obtained from the A/D converter each time it is sampled by the A/D clock. This rate is appropriately chosen to accommodate the modulation and its characteristics (particularly “bandwidth”) of the information to be received.

The “noise model” used for the simulation of the “stream” of signal-to-noise trials is based on generally accepted Gaussian type of probability density distributions as used on radar and communications receiving systems. While such distribution is significant in analytical treatments, the non-real time methods used here are less susceptible to the noise model. This is because each unwanted noise sample is literally forced to a value that goes through zero at each point of inflexion. This is controlled by its relative positioning in the “topographic array”.

As a result of the above steps, each trial has a unique column whose relative location in the network corresponds to the magnitude of the noise portion of that trial and whose + or – polarity location is opposite that of the actual noise polarity. Thus, the “noise entry” in the matrix will transition through zero in such a correlated column.

To illustrate this, Figure 4(a) and (b) was constructed using the simulated values of the noise. (These are not available in practice but serve here merely to illustrate the nature and effectiveness of the array of columns to accurately “locate” the noise within the topographical matrix.)

5 To extract the information (as to column choice) it is important that part of the information is introduced or “scanned” into the iterative matrix in a special way that will produce a “proper error sense” when making voltage comparison between entries from two appropriate columns. The pertinent columns are either of the first or second trials and the average of these two trials. To accomplish this, the “average row” is scanned
10 (i.e., the voltages introduced) in a minus to plus manner, which is the opposite of that used in trial 1 and trial 2, as shown in FIG. 5(a). This insures that the error sense at the different “zero noise transition points” are opposite rather than “parallel”, i.e., having like slopes as illustrated in Figure 5(b). The appropriate “zero noise comparisons” are made between each trial and the average. Such comparisons can locate the column location to
15 a high degree of sharpness or precession using interpolations of the values from adjacent columns.

The deviations from the average are used because of two or more trials, i.e., samples of signal plus noise are averaged, then the algebraic sum of the two or more deviations from the average is zero. This concept is one of the foundations of making the
20 process independent of signal level, i.e., the deviation from the average contains no signal and is expressed as 1A or QA. (The “deviation from Average” is simply equal to the actual I (or Q) minus the average I (or Q) of the two (or more) of trials.) Since both I and

I average contain the signal, the subtraction of the average I from the actual I cancels the signal.

The topological number array is rendered a change detector by applying a column shift process in which this shift is equal in amount to the magnitude of the deviation and the shift direction, i.e., left or right, is determined by the polarity of the deviation. The amount of shift is the deviation amplitude divided by the column spacing increments to express the result in number of columns. This amount of shifts is made in the “deviation from average row” and places the two rows (the deviation from average row and the average row) in equilibrium about the zero column, which is the topographic column. An equilibrium condition, such as shown in Fig 6, qualifies the matrix as a change detector because any further disturbances in either row introduced by an iterative probe will create a mismatch of column readings and lead to a new location for the match of the column entries; such a new match will occur in either the left or right portion of the topological array.

A flow diagram is shown by Fig. 9 and Fig. 10 consisting of the logical selection for each iterative probe, Fig 9, and the control of the iterative steps, Fig 10.

Starting with the condition given in Fig 8 which contains the instructions for obtaining the initial column match, the consequences of such a match are determined by the decision logic in Fig 9. The first determination is whether the “new” match (caused by the initial iterative probe) occurs in the left or in the right portion of the topographical number array sensor. The next question resolved is whether or not this situation represents a change in side with respect to its initial location (i.e. from left to right or vice versa). A “yes” in either indicates that a change in polarity has occurred indicating the

use of the new polarity for the next iteration. In recognition that the first iteration was sufficient to cause such a significant change, the next probe should be of a smaller amount and the diagram shows the former value is halved to cause the match from the next probe to occur closer to zero.

5 The absence of a change of polarity (i.e. same side location) indicates that a probe of the same polarity as the previous one should be continued for the next probe.

However, it is now desired to know whether the prior probe caused the resulting column match to occur closer to, or farther from zero. The closer the match is to zero is an indication that the process is converging and a smaller value (such as one half) should be a good choice unless it causes "overshoot" (i.e. change of polarity on the next iterative probe). However, if this probe is not halved and a large amount of noise is present, the process should converge faster, until the polarity changes; if it is found that more than 2 iterations result in continued maintenance of the same polarity; if this occurred the 3rd and or 4th iteration will benefit by not continuing to halve of the magnitude of the next probe. This will occur until a polarity change is noted. Such downstream iterations are shown in Figure 11 which is referred to as "augmented logic" reflecting iteration history.

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20 If the consequences of the process makes the match farther from zero, a divergence is indicated which calls for the next probe value to be of opposite polarity and greater than 1 to make up for the loss of convergence during this probe. A nominal value such as 1.5X for the next iteration is shown on the diagram of Fig 9.

Using such logic, the choice of one of six different options available is indicated in the form of an appropriate magnitude and polarity for the next probe.

It should be perceived that the selections of a series of appropriate probes as illustrated in Fig 9 through Fig 11 are representative of the process that determines the “speed” of convergence to use a smaller number of iterations to cope with the larger value of noise the magnitude selections process might eliminate the ½ where a question mark is shown.

Figure 12 (a) and (b) show a computer printout of typical results of the process illustrated by Figures 9 and 10 using appropriate iterative programming to achieve the results shown. These represent the results for each trial of converging results show by the middle (and next to last column), of the noise values after each of six iterative steps. The “original” average noise for each trial is shown in the first column after the trial number, for 36 independent trials (3 per entry number) for I’s, (Figure 12(a)) and Q’s, (Figure 12 (b)). (The I and Q results have been processed independently).

The key results are shown in the “Equivalent voltage added” column which is the algebraic sum of all the plus and minus voltage probes all of the iterations and represent the “output” as shown previously in Figure 10. This column provides the sought-after estimate of the magnitude of the noise, note that these values closely approximate the magnitude of the actual noise show in the first column. The polarity of this magnitude will be opposite as shown clearly in the printout. The ratios of these estimated magnitude values to the original are shown in the last column. These vary widely although the estimate values as very close to the actual as expressed by the residual noise in the nest to the last column. The ratio column is in terms of voltage comparison so that a ratio of 10 corresponds to a “20 dB” improvement.

The noise residuals are generally within $\pm .02$ volts. This value is determined for the most part by the number of iteration and will diminish to a value ultimately determined by the accuracy of the digital measuring ability of the process. Which will depend on how well the embodiment is executed.

5 The ratio must be interpreted carefully because frequently the lower ratio corrupted to noise that is already low relative to the "norm". Taking this into account perusal of the result indication an integrated improvement of about 30 dB; with one or two more iteration this improvement would improve by 6 or 8 dB.

10 USE OF INTEGRATED CIRCUITS

The operations previously described can be implemented by means of integrated circuit "chips"; such a semi-conductor integrated circuit first provides the means for injecting a series of predetermined digital values furnished by, for example, preprogrammed Electrically Programmed Read Only Memory (EPROM) that also
15 memorize the resulting "new" digital values. The result is a stored topographical number matrix of two rows which can serve as a means of sensing changes in each step of an iterative process or 4 or more steps. Each step includes an iterative probe, which cause a column displacement that is determined by its magnitude and polarity. The information in two appropriate columns is compared by a digital number compared to obtain a match
20 when these entries are approximately equal. This is in accordance with Figures 2 and 7.

As a result of the location of this match the next iterative value prove is determined by using the logic shown in Figure 9. Such a new probe value consists of its magnitudes and polarity. This process is repeated for each of the several iterations and

the algebraic summation of the probe values the “chips: with an accurate estimate of the noise portion in the form of a magnitude and a polarity (the latter is opposite to that of the noise.) This permits a nearly complete noise cancellation from the stored (and delayed original signal plus noise sample for each trial. As a result of the iterative converging process on the chip each trial provides a “frame of enhanced signal information.” A series of such trials or samples accommodate the modulations of the signal to provide a stream of modulated signals.

It should be noted that in the above process key information from the decision tree of Figure 9 is given as to whether, after each iterative probe the column match occurs either closer to or further from the center column.

Each iteration starts with the conditions from the end of the previous one and each series provides a frame of information to accommodate signal modulation. Several chips (or subsection of one chip) can be used in a form of parallel processing of different complete iterative frames. One or more such frame can be separately and simultaneously formed and stored to increase the speed of processing of each frame.

For each entry, the column choice is employed to carry out the process to obtain the estimate for each trial. The value readout can be determined more accurately by interpolation between adjacent column. This process can provide a precision of determination of about .01 volts as determined digitally by the column readings described next. A voltage of such precision is subtracted algebraically from each noise sample in an ongoing manner to provide a continuous stream of information from which the noise has been dramatically reduced.

The "Column readers" shown in Figure 2 provide two different types of information. The first is used to help locate the relative positions of the columns that contain the pertinent information. This requires a "match" of the readings between two entries in these two columns. The second is the value of the column value calibration as determined by its location.

The ability to sense a smaller value can be enhanced if the signal plus noise "voltage" range is increased, by amplification to ± 3 or ± 5 volts. This is in terms of digital values. To this end, the same " ± 1 volt chip" can be time shared 3 or 5 times to provide segmented coverage of the total range of appropriate sequential bias values for each replication. This approach of course, when performed "offline", will increase the time delay imposed by the processing and thereby influence the "speed" requirement of the processing chips. Storage capacity is provided to accomplish the expanded iterative network (or matrix) coverage so as to permit the access to be performed.

INTERNET SYSTEM CONFIGURATION

Figure 1(a) shows a simplified but comprehensive representation of the overall scheme used to provide a communication system suitable for the Internet. The key elements shown in addition to "the sender" and the "receivers" (by stations or by individual users) are 1) the "Service Provider" facilities, 2) an overall network for "Switching and Routing," and 3) Localized Distribution means.

The key functioning elements in this overall network are the "gateways" at the entrance of the Service Provider and the gateways of the Localized Distribution System to which the message (coded as to distribution) is routed; the gateway of the ultimate user

is the remaining link of the process. Shown are the means of using analog information at the gateways and eventually using the received information at the user also in analog form. This is the result of using messages historically at audio frequencies (sometimes involving a “carrier” as well).

5 These capabilities will need to go beyond historical practice when the information is expanded to include data used for business and special function beyond “voice” and with an even greater demand when video frequencies are accommodated.

10 Figure 1(b) illustrates an embodiment of the invention at a gateway receiving the signal in analog forms (at audio or video frequencies). Sometimes a carrier frequency is used, which is modulated in various ways by such frequencies. Figure 1(b) represents the invention in its more basic form.

15 Figure 1(c) illustrates an embodiment for which a auxiliary step is required which can be provided, for example, by a modem, when receiving a signal in digital form and which can occur in digital packets of information which have been “compressed” as part of the bandwidth accommodation characteristics of the network. In such an instance a decompression means is used before a digital to analog conversion.

 Figure 1(b) is referred to for simplicity of explanation, as an “A/D gateway” while Figure 1(c) is called a “D/A gateway”.

20 The roles and function of the invention can be explained in such use by reference to the overall system scheme illustrated as Figure 1(c); accordingly.

 The Service Provider receives the many separate signals from many senders with such signal being accommodated by gateways which in the instance should employ the embodiment of the invention shown in Figure 1(b) to provide an enhanced signal in

digital form as shown in the diagram. This implementation is a simplified block diagram of the more comprehensive block diagram of Figure 2 that has been explained previously.

The total process including the iterative probing, sensing and decision making using feedback method for several iterations or steps and these are referred to as the one-
5 block "Iterative Processor". Such a processor provides an accurate noise estimate for each trial and this is "subtracted" from each signal-plus-noise sample to remove most of the actual noise; this step requires an appropriate (fixed) time delay to correlate or align, corresponding samples. As explained throughout this specification the processing occurs in "near real-time" to provide the opportunity for the signal-to-noise enhancement. Such enhancement takes place between points A & B so that an enhanced signal is furnished to
10 the "Multiplexing" and Assignment shown within the Service Provider block. The multiplexing permits more than one "message" to be carried on a single line, which can be a wire or fiber optic strand.

At point B this enhancement of relative signal strengths could be 30 dB or more
15 relative to the noise that would be present without this embodiment and such an improvement can be used, in part to provide more effective multiplexing to achieve greater channel density. An alternative to using all, or part of the "30 dB" improvement would be the ability to accept weaker signals so that signals from a farther distance away could be accommodated. A typical allocation might be 10 dB for longer "range" and 20
20 dB for more channel capacity for the same basis of the Service Provided signal to the switching and routing network. Such a signal might be provided in "packets" of digital information that have undergone compression of modulated information. This process

occurs after the enhancement and the primary role of Figure 1(b) is to provide a stronger signal.

The switching and routing network has a wide range of technology using wire and fiber optics in accordance with an "internet protocol" that sends the signals to the
5 Localized Distribution System. The gateway at the Localized Distribution System would use the embodiment of the invention as augmented by the addition as shown in Figure 1(c); here the signal received as a result of routing consisting of compressed packets that require decompression before the digital to analog conversion. Because of the enhancement potential of the invention a smaller signal can be accepted here, relative to
10 noise. For a given acceptable digital error rate a strong analog signal is delivered to the Multiplexing portion of the Distribution system. This improvement can enable such multiplexing to accommodate more channels (i.e. increased channel capacity) here as well as in previous multiplexing.

Such a signal is delivered to the final gateway at the receiver of the user; here the
15 version of Figure 1(b) is used again. The enhancement now permits a weaker receive signal (relative to noise) to be received. Those enhancements can be used to extend the range to the user as well as help accommodate the addition channel provided at the distribution system by the enhancement of gateway #2 (Figure 1(c). The enhanced signal resulting from gateway 3 can be used to provide a stronger signal that will facilitate
20 realization of a shorter time to acquire (i.e. access) the Internet connection and help the "last mile" of the reception link.

What is claimed is:

1. A method for increasing the signal to noise ratio of a receive wireline system, said method comprising the steps of:

- receiving receive signals from a wire-line;
- amplifying said receive signals to form amplified signal-plus-noise signals;
- 5 creating in-phase and quadrature digital versions of said received signals wherein said in-phase and quadrature versions are about ninety degrees out of phase with respect to each other;
- storing said signal-plus-noise signals in a memory device;
- forming at least one matrix digitally representing a plurality of values, said values
- 10 consisting of said in-phase and quadrature versions of said receive signals;
- performing an iterative process on data contained in said matrix to determine an estimate of the magnitude and polarity of the noise portion of the signal-plus-noise for each trial; and
- subtracting each estimated noise value from the stored signal-plus-noise version to obtain a noise-reduced signal.

2. A method as claimed in claim 1 further comprising:

- forming left and right topological groupings of digital numbers about a topocentric reference that corresponds to a zero voltage injection from pre-programmed and memorized voltage value injection patterns that comprise incremental successively
- 5 increasing positive and negative steps in each of a plurality of rows, each row having similar increments with the same topocentric zero reference.

3. A method as claimed in claim 1 further comprising:

- using a topographic digital number array, that covers a positive and negative (i.e. bipolar) range and is in equilibrium about a topocentric value, to detect when the polarity of the noise portion of a signal-to-noise combination changes from positive to negative or
- 5 from negative to positive in response to an injection of a predetermined value probe.

4. A method as claimed in claim 1, wherein said iterative processing comprises:

sequentially applying a series of digital value probes to said data to alter a value representing signal-plus-noise and wherein several iterations produce an estimate of a noise portion of the signal-plus-noise by algebraically summing resultant values of the several iterative steps.

5. An iterative value programmer operable to provide digital value steps, or probes, used in conjunction with a sensor operable to sense a change caused by each step or probe in a bipolar fashion, wherein an amount of said change is determined for both positive and negative values of a noise component of signal-plus-noise samples in a symmetric fashion.

6. A method as claimed in claim 4, further comprising:
providing at least one of the rows pattern of aforementioned pre-programmed plus and minus values that is reserved in a pre-programmed manner such as to cover the column injectors from minus to plus instead of the aforementioned plus to minus but in a similar pattern except for the polarity sense;
opposite polarity "senses" provide sharper the error responses of column difference to yield comparison.

7. A method as claimed in claim 2, further comprising:
forming a topographical number array rendered in equilibrium, and symmetrical about the topocentric zero reference, by shifting a row of the array corresponding to a signal-to-noise entry that has a minimum deviation of said entry from the average of the two or more entries, such average referenced as a first row and these two aforementioned rows having the plus and minus increment patterns reversed with respect to each other.

8. A method as claimed in claim 1, further comprising
providing a processing means for performing said iterative processing wherein bandwidth and signal handling capabilities of the system are not adversely compromised

and wherein a time delay of said processing means is short with respect to said method;
and

utilizing the short time delay to permit signal-to-noise to be significantly improved.

9. A method as claimed in claim 4, further comprising:

providing time needed to perform the iterative process by thereby realizing means for achieving "near-real time" behavior of the sensing system by executing the iterations at a slower rate than the basic receipt of signal information, which corresponds to the "Nyquist" sampling rate, which is in accordance with the signal modulation characteristics, such iterative process having several iterations accomplished at a fast processing speed, wherein the iterations occur while the received samples are stored and remembered while the several iterations take place and wherein the desired relative processing speed is controlled by the division of the sampling frequency as determined by an advisor ratio, thereby achieving a prescribed known rate and a fixed tolerable time delay.

10. An apparatus operable to accomplish the method of claim 4 wherein sensing and control abilities of the topographical number array are needed to execute the converging iterative process, said apparatus being enabled by the delay and storage features that maintain the sign apportion of this process constant so as to render the variations that occur from one iterative to the next one to consist primarily of the noise changes.

11. An integrated circuit device comprised of means of performing primary simple functions namely digital addition (or subtraction) to form a topological array matrix consisting of two or more rows and a plurality of contiguous left hand, and right hand, columns which together with a means of utilizing column shifting (as controlled by an iterative programmer) so as to provide from the chip a "bipolar" means of sensing of the consequences of each iterative probe value supplied by such a program with these

consequences being interpreted equally well without regard for the net polarity of the noise portion of each signal-to-noise sample.

12. An iterative programmer in accordance with claim 5, further comprising:
an integrated circuit device consisting of a chip, or a portion of a larger chip, that
can interpret the response of each iterative probe to be used to help control said
programmer so as to determine the magnitude and polarity of a subsequent probe, with
each such decision made by a logic flow process.

13. An iterative programmer in accordance with claim 5, further comprising:
an integrated circuit device consisting of one or more chips, or a portion of a large
chip, operable to execute the series of steps that constitute the iterative process so as to
converge in a manner that provides an accurate noise estimate for each trial in accordance
with said iterative process.

14. An integrated circuit device on a chip, or group of chips, that hosts a
specially structured numerical array or matrix as defined by claim 3 in which computed
deviations from array values, which are signal level independent, are applied to one row
of said matrix in the form of a plus or minus column shift results in the matrix being in
equilibrium about the topocentric (the zero column) of the array and thereby enduring the
matrix with the ability to serve as a change detector to sense progressive changes as
caused by a series of iterative probes.

15. An integrated circuit chip as claimed in claim 14 that executes a logic flow
guided by means of a decision tree and thus, in an orderly fashion, reduces six possible
consequences to a single choice of one value for a subsequent iterative probe, such choice
consisting of an appropriate magnitude and polarity.

16. An integrated circuit chip, or aggregate of chips, that performs an iterative
process by using iterative probes (magnitude and phase) where consequences are
determined by the decision logic results of claim 1 in a series of iterative steps each

assessed as to topological changes so as to resulting in selection of an appropriate next
5 probe value to cause a series of iterations that converge to a near zero conclusion and
providing an algebraic sum which is a close approximation tot he equivalent noise value,
in digital form, which can be subtracted from the signal-to-noise value of each trail.

17. A device in accordance with claim 15, further comprising:

a decision device operable to augment the decisions made for the early iterations
by coupling some of the results from later iteration results back to the decision processfor
possible modifications in determining the magnitude of such iterative probe used in
5 middle and later iteration based on a cumulative history from such iterative process.

18. A receive system consisting of an arrangement of devices in accordance
with claim 11, wherein said system further provides an output signal that is enhanced
considerably with respect to the inherent noise that is present without such devices and
arrangements and with such enhancement manifest in the strength of the carrier signal in
a communication system.

19. A receive system in accordance with claim 18 further operable to
accommodate and interpret various forms of modulation of the carrier of said signal, such
an ability being achieved by a succession of frames of information that are generated in
near-real time to retrieve the modulated signal information that is less corrupted by said
noise.

20. A receive system in accordance with claim 19, further comprising:

an integrated circuit device capable of providing said frames of information to
work in one or more pairs to form a paralleled processing arrangement in which
separately remembered signal frame(s) can be captured and stored simultaneously so that
5 the output of each can be utilized individually and serially to contract the desired noise-
reduced signal by successive frames that provide the modulation characteristics of the
sequence, all of this being done in a tolerably short and predetermined fixed time which
is manifested as signal delay, without comprising bandwidth.

21. A method as claimed in claim 8, further providing a practical implementation of a non-stationary series of events that are executed in non-real time by an iterative probe and unique bipolar sensing method that result in improving the entropy of the system.

22. A method as claimed in claim 1 further comprising:

implementing a comprehensive method of realizing near-real time processing that satisfies the "second law" of thermodynamics by achieving, during a tolerable known time departure (i.e. fixed "time delay") from real time, an estimate of the noise portion of the signal plus noise of said iterative process, said estimate serving as a statistical
5 mechanic results such that when such a quantity is subtracted, it is analogous to an introduction of energy at a lower temperature in a thermal system, thereby improving (i.e. lowering) the effective entropy of each trial.

23. Means of enhancing signal outputs provided from a gateway of a service provider, such enhanced outputs being provided in a digital format as a result of an overall iterative process which substantially lowers an amount of internal noise normally present with the signal, such enhancement being able to improve a next process that receives such a signal to improve a source error rate, a realizable channel density and a multiplexing performance used to route information.

24. A device operable to enhance signals received at gateways that are part of a localized distribution area in a form that are in packets (with destination labels) in which such digital information is changed to analog from (with decompression if necessary) and converted with a digital to analog device to reconstruct an analog signal
5 which is then converted to digital from by processing where both the signal and the locally generated noise are present in an interwoven combination to which an iterative processing scheme is applied to provide further relative enhancement of the signal by minimizing such noise.

25. The device as claimed in claim 24 further comprising:

an interpreter operable to interpret the digitally represented signal more reliably and with a lower error rate, wherein enhanced performance results which can be traded-off for the same acceptable error rate to translate the improvement for higher channel density and/or longer range reception.

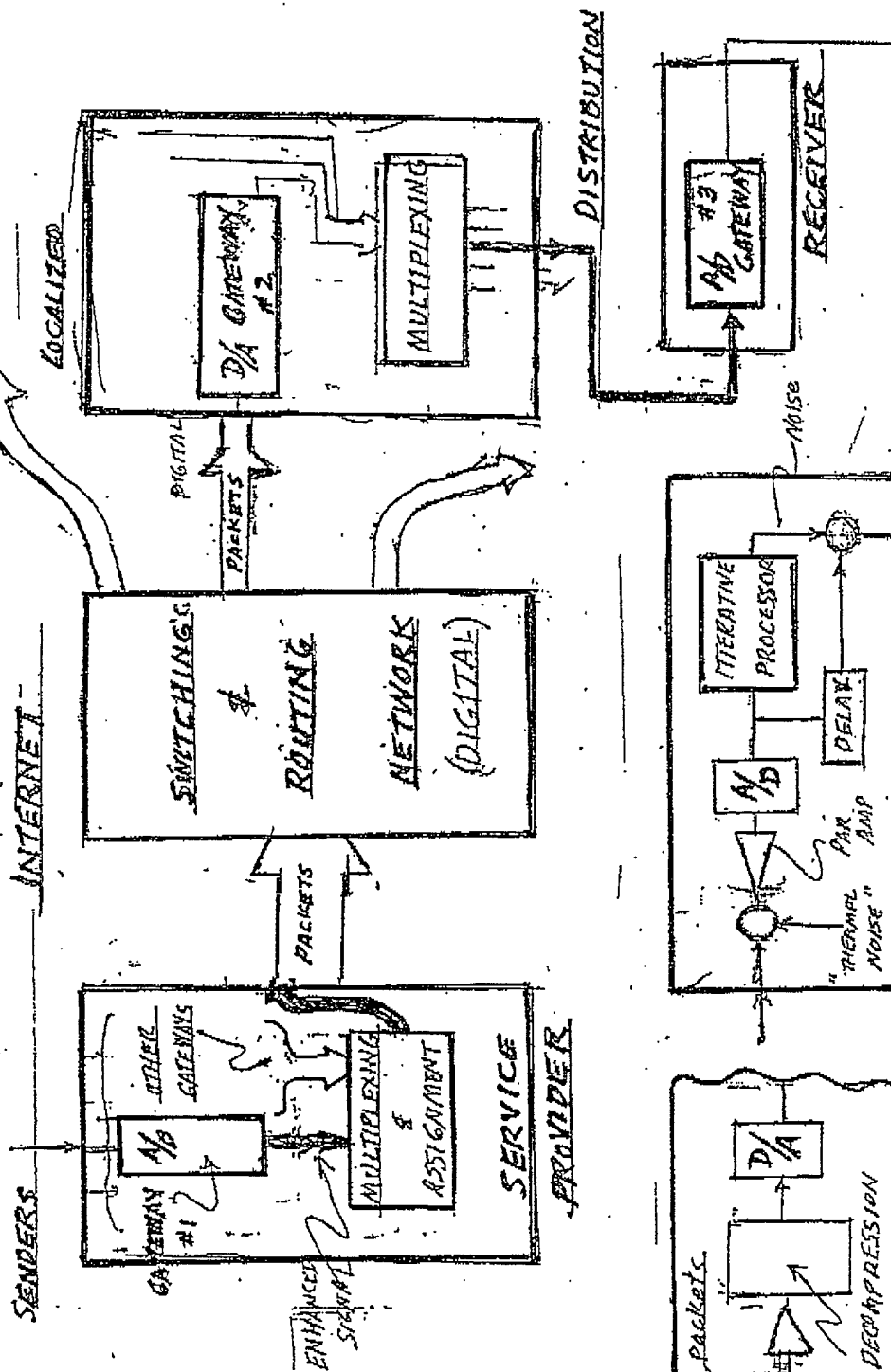
26. A method as claimed in claim 1 wherein said method enhances the receive signal at a gateway of an individual user, such improvement consisting of a stronger signal, relative to noise, at a user end of the overall process providing a longer communication distance and/or quicker access time potential.

27. A method of realizing a cascading multiple stage improvement of an overall information control and distribution system using signal-to-noise improvement manifested in a variety of embodiments based in principals as described for the invention in the various forms herein the aggregated overall improvements potential can be used to help optimize the overall, as well as the individual subsystems parts, or the overall system in a way that can improve performance parameter such as channel capacity, shorter access time, better range and reliability, that are achieved in part by the increased multiplexing options

ABSTRACT OF THE DISCLOSURE

A receive system providing enhanced Signal to Noise performance is applicable to a wide variety of applications including both wireless and wireline systems which further include internet type communications. Received signals are converted to digital values and stored in a manner which enables subsequent processing directed to improving the resolution of the received signals and to reduce the associated noise corresponding to the received data samples. The Signal-to-Noise ratio of the received data signals is improved as a result of processing techniques made possible by the digitally stored nature of the received data and a unique iterative data processing method.

FIG 1 ENHANCEMENT OPPORTUNITIES



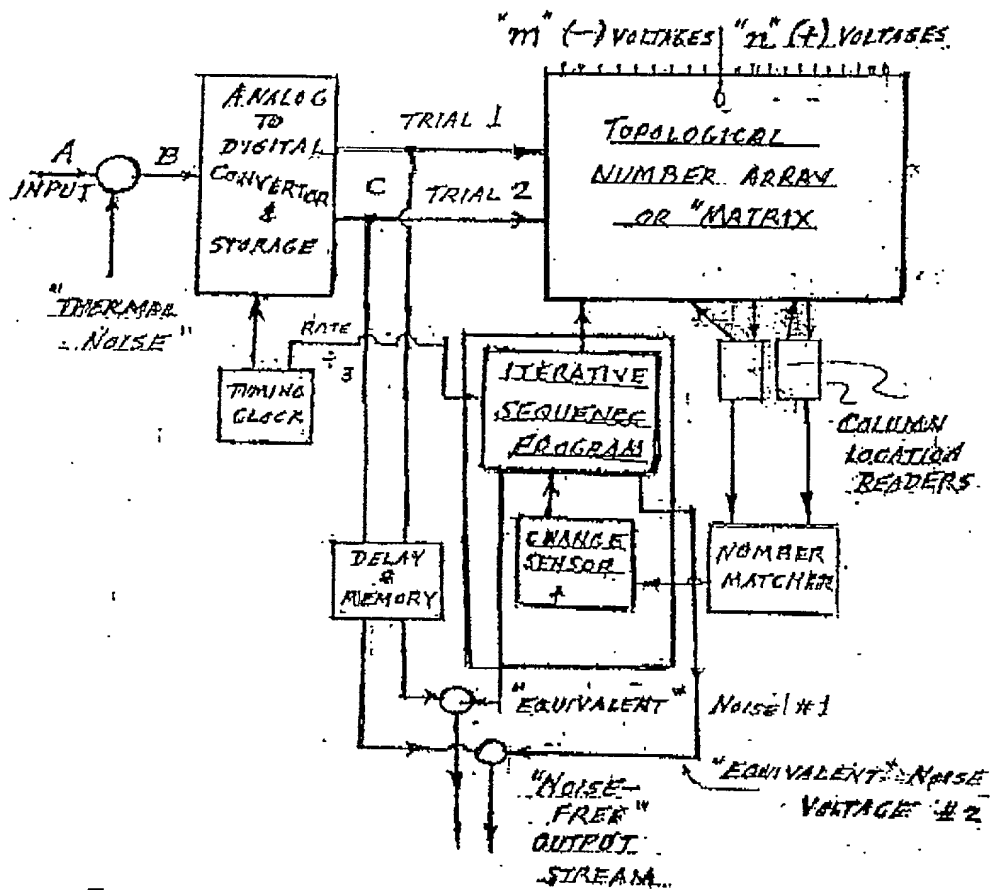


FIG 2 BLOCK DIAGRAM

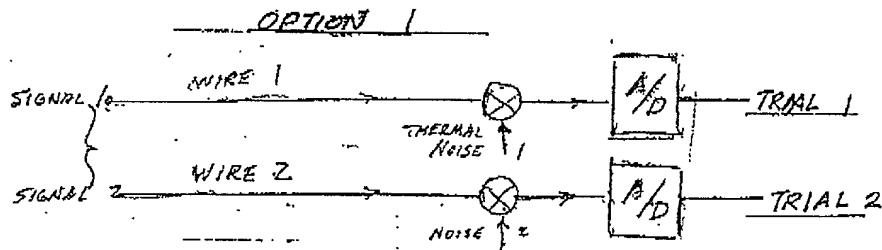


FIG 3 (a) 2-WIRE (SAME SIGNAL - 2 NOISES)

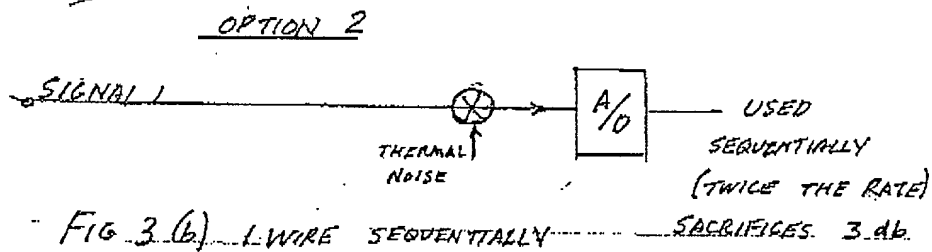


FIG 3 (b) 1-WIRE SEQUENTIALLY

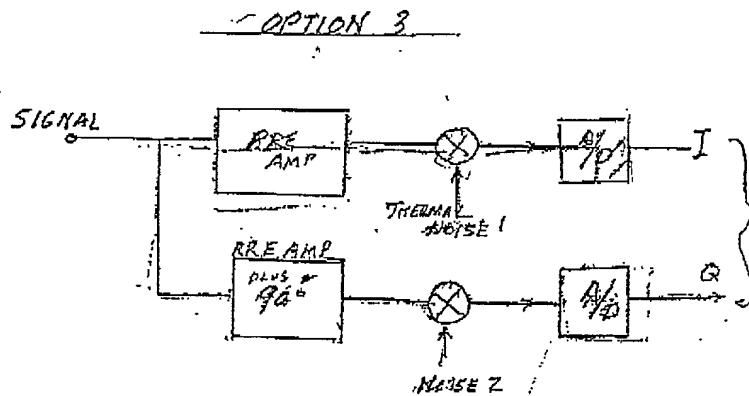


FIG 3 (c) 1-WIRE USING IN PHASE I AND QUADRATURE Q

FIG 3 CONNECTION OPTIONS

I data ---- Group 1 82M Noise averages 820 *** Avg scanned in opposite sense ***

	Min 1A	-1.5 W	-1.0 W	-0.5 W	0 W	0.5 W	1.0 W	1.5 W	2.0 W	2.5 W	3.0 W	3.5 W	4.0 W	4.5 W	5.0 W	5.5 W	6.0 W	6.5 W	7.0 W	7.5 W	8.0 W	8.5 W	9.0 W	9.5 W	10.0 W
Avg	1.306	1.156	1.104	1.056	1.004	0.956	0.904	0.856	0.804	0.756	0.706	0.656	0.606	0.556	0.506	0.456	0.406	0.356	0.306	0.256	0.206	0.156	0.106	0.056	0.006
200	0.041	-0.552	-0.502	-0.452	-0.402	-0.352	-0.302	-0.252	-0.202	-0.152	-0.102	-0.052	-0.002	0.048	0.098	0.148	0.198	0.248	0.298	0.348	0.398	0.448	0.498	0.548	0.598
Avg	-0.671	0.541	0.591	0.641	0.691	0.741	0.791	0.841	0.891	0.941	0.991	1.041	1.091	1.141	1.191	1.241	1.291	1.341	1.391	1.441	1.491	1.541	1.591	1.641	1.691
210	-0.652	-1.151	-1.111	-1.061	-1.011	-0.961	-0.911	-0.861	-0.811	-0.761	-0.711	-0.661	-0.611	-0.561	-0.511	-0.461	-0.411	-0.361	-0.311	-0.261	-0.211	-0.161	-0.111	-0.061	-0.011
Avg	0.735	0.685	0.635	0.585	0.535	0.485	0.435	0.385	0.335	0.285	0.235	0.185	0.135	0.085	0.035	0.015	0.065	0.115	0.165	0.215	0.265	0.315	0.365	0.415	0.465
220	0.040	-1.095	-0.955	-0.905	-0.855	-0.805	-0.755	-0.705	-0.655	-0.605	-0.555	-0.505	-0.455	-0.405	-0.355	-0.305	-0.255	-0.205	-0.155	-0.105	-0.055	-0.005	0.045	0.095	0.145
Avg	0.654	0.604	0.554	0.504	0.454	0.404	0.354	0.304	0.254	0.204	0.154	0.104	0.054	0.004	0.044	0.094	0.144	0.194	0.244	0.294	0.344	0.394	0.444	0.494	0.544
230	0.022	-1.121	-1.074	-1.024	-0.974	-0.924	-0.874	-0.824	-0.774	-0.724	-0.674	-0.624	-0.574	-0.524	-0.474	-0.424	-0.374	-0.324	-0.274	-0.224	-0.174	-0.124	-0.074	-0.024	0.026
Avg	1.164	1.116	1.064	1.014	0.964	0.914	0.864	0.814	0.764	0.714	0.664	0.614	0.564	0.514	0.464	0.414	0.364	0.314	0.264	0.214	0.164	0.114	0.064	0.014	0.046
240	-0.002	-0.637	-0.587	-0.537	-0.487	-0.437	-0.387	-0.337	-0.287	-0.237	-0.187	-0.137	-0.087	-0.037	0.013	0.063	0.113	0.163	0.213	0.263	0.313	0.363	0.413	0.463	0.513
Avg	1.100	1.050	1.000	0.950	0.900	0.850	0.800	0.750	0.700	0.650	0.600	0.550	0.500	0.450	0.400	0.350	0.300	0.250	0.200	0.150	0.100	0.050	0.000	0.040	0.090
250	-0.032	-0.732	-0.682	-0.632	-0.582	-0.532	-0.482	-0.432	-0.382	-0.332	-0.282	-0.232	-0.182	-0.132	-0.082	-0.032	0.018	0.068	0.118	0.168	0.218	0.268	0.318	0.368	0.418
Avg	0.467	0.417	0.367	0.317	0.267	0.217	0.167	0.117	0.067	0.017	-0.033	-0.083	-0.133	-0.183	-0.233	-0.283	-0.333	-0.383	-0.433	-0.483	-0.533	-0.583	-0.633	-0.683	-0.733
260	-0.153	-1.463	-1.413	-1.363	-1.313	-1.263	-1.213	-1.163	-1.113	-1.063	-1.013	-0.963	-0.913	-0.863	-0.813	-0.763	-0.713	-0.663	-0.613	-0.563	-0.513	-0.463	-0.413	-0.363	-0.313
Avg	0.924	0.874	0.824	0.774	0.724	0.674	0.624	0.574	0.524	0.474	0.424	0.374	0.324	0.274	0.224	0.174	0.124	0.074	0.024	-0.026	-0.076	-0.126	-0.176	-0.226	-0.276
270	-0.120	-0.754	-0.704	-0.654	-0.604	-0.554	-0.504	-0.454	-0.404	-0.354	-0.304	-0.254	-0.204	-0.154	-0.104	-0.054	0.004	0.054	0.104	0.154	0.204	0.254	0.304	0.354	0.404
Avg	0.782	0.732	0.682	0.632	0.582	0.532	0.482	0.432	0.382	0.332	0.282	0.232	0.182	0.132	0.082	0.032	0.002	0.052	0.102	0.152	0.202	0.252	0.302	0.352	0.402
280	-0.176	-0.840	-0.790	-0.740	-0.690	-0.640	-0.590	-0.540	-0.490	-0.440	-0.390	-0.340	-0.290	-0.240	-0.190	-0.140	-0.090	-0.040	0.010	0.060	0.110	0.160	0.210	0.260	0.310
Avg	1.246	1.196	1.146	1.096	1.046	0.996	0.946	0.896	0.846	0.796	0.746	0.696	0.646	0.596	0.546	0.496	0.446	0.396	0.346	0.296	0.246	0.196	0.146	0.096	0.046
290	-0.129	-0.683	-0.633	-0.583	-0.533	-0.483	-0.433	-0.383	-0.333	-0.283	-0.233	-0.183	-0.133	-0.083	-0.033	0.017	0.067	0.117	0.167	0.217	0.267	0.317	0.367	0.417	0.467
Avg	0.848	0.798	0.748	0.698	0.648	0.598	0.548	0.498	0.448	0.398	0.348	0.298	0.248	0.198	0.148	0.098	0.048	0.008	0.058	0.108	0.158	0.208	0.258	0.308	0.358
300	0.032	-0.921	-0.871	-0.821	-0.771	-0.721	-0.671	-0.621	-0.571	-0.521	-0.471	-0.421	-0.371	-0.321	-0.271	-0.221	-0.171	-0.121	-0.071	-0.021	0.029	0.079	0.129	0.179	0.229
Avg	0.706	0.656	0.606	0.556	0.506	0.456	0.406	0.356	0.306	0.256	0.206	0.156	0.106	0.056	0.006	0.046	0.096	0.146	0.196	0.246	0.296	0.346	0.396	0.446	0.496
310	-0.174	-1.167	-1.117	-1.067	-1.017	-0.967	-0.917	-0.867	-0.817	-0.767	-0.717	-0.667	-0.617	-0.567	-0.517	-0.467	-0.417	-0.367	-0.317	-0.267	-0.217	-0.167	-0.117	-0.067	-0.017
Avg	1.040	1.010	0.960	0.910	0.860	0.810	0.760	0.710	0.660	0.610	0.560	0.510	0.460	0.410	0.360	0.310	0.260	0.210	0.160	0.110	0.060	0.010	0.040	0.090	0.140
320	-0.015	-0.755	-0.705	-0.655	-0.605	-0.555	-0.505	-0.455	-0.405	-0.355	-0.305	-0.255	-0.205	-0.155	-0.105	-0.055	0.005	0.055	0.105	0.155	0.205	0.255	0.305	0.355	0.405
Avg	0.933	0.883	0.833	0.783	0.733	0.683	0.633	0.583	0.533	0.483	0.433	0.383	0.333	0.283	0.233	0.183	0.133	0.083	0.033	-0.017	-0.067	-0.117	-0.167	-0.217	-0.267
330	-0.050	-0.897	-0.847	-0.797	-0.747	-0.697	-0.647	-0.597	-0.547	-0.497	-0.447	-0.397	-0.347	-0.297	-0.247	-0.197	-0.147	-0.097	-0.047	0.003	0.053	0.103	0.153	0.203	0.253
Avg	0.530	0.480	0.430	0.380	0.330	0.280	0.230	0.180	0.130	0.080	0.030	0.000	-0.050	-0.100	-0.150	-0.200	-0.250	-0.300	-0.350	-0.400	-0.450	-0.500	-0.550	-0.600	-0.650
340	-0.203	-1.470	-1.420	-1.370	-1.320	-1.270	-1.220	-1.170	-1.120	-1.070	-1.020	-0.970	-0.920	-0.870	-0.820	-0.770	-0.720	-0.670	-0.620	-0.570	-0.520	-0.470	-0.420	-0.370	-0.320
Avg	1.075	0.925	0.875	0.825	0.775	0.725	0.675	0.625	0.575	0.525	0.475	0.425	0.375	0.325	0.275	0.225	0.175	0.125	0.075	0.025	0.005	0.055	0.105	0.155	0.205
350	-0.083	-0.648	-0.598	-0.548	-0.498	-0.448	-0.398	-0.348	-0.298	-0.248	-0.198	-0.148	-0.098	-0.048	0.002	0.052	0.102	0.152	0.202	0.252	0.302	0.352	0.402	0.452	0.502
Avg	1.171	1.121	1.071	1.021	0.971	0.921	0.871	0.821	0.771	0.721	0.671	0.621	0.571	0.521	0.471	0.421	0.371	0.321	0.271	0.221	0.171	0.121	0.071	0.021	0.041
360	-0.212	-0.841	-0.791	-0.741	-0.691	-0.641	-0.591	-0.541	-0.491	-0.441	-0.391	-0.341	-0.291	-0.241	-0.191	-0.141	-0.091	-0.041	0.009	0.059	0.109	0.159	0.209	0.259	0.309
Avg	1.024	0.974	0.924	0.874	0.824	0.774	0.724	0.674	0.624	0.574	0.524	0.474	0.424	0.374	0.324	0.274	0.224	0.174	0.124	0.074	0.024	0.004	0.054	0.104	0.154
370	0.015	-0.741	-0.691	-0.641	-0.591	-0.541	-0.491	-0.441	-0.391	-0.341	-0.291	-0.241	-0.191	-0.141	-0.091	-0.041	0.009	0.059	0.109	0.159	0.209	0.259	0.309	0.359	0.409
Avg	0.516	0.466	0.416	0.366	0.316	0.266	0.216	0.166	0.116	0.066	0.016	0.006	-0.044	-0.094	-0.144	-0.194	-0.244	-0.294	-0.344	-0.394	-0.444	-0.494	-0.544	-0.594	-0.644
380	0.003	-1.191	-1.141	-1.091	-1.041	-0.991	-0.941	-0.891	-0.841	-0.791	-0.741	-0.691	-0.641	-0.591	-0.541	-0.491	-0.441	-0.391	-0.341	-0.291	-0.241	-0.191	-0.141	-0.091	-0.041

FIG 4(a)

-0.05	0	.05	.1	.15	.2	.25	.3	.35	.40	.45	.5	.55	.6	.65	.7	.75
0.354 0.299	0.394 0.348	0.355 0.309	0.335 0.448	0.355 0.429	0.404 0.546	0.453 0.595	0.502 0.649	0.551 0.692	0.599 0.742	0.648 0.788	0.697 0.839	0.746 0.899	0.795 0.945	0.844 0.999	0.893 1.048	0.942 1.096
-0.159 -0.311	-0.302 -0.261	-0.259 -0.211	-0.309 -0.161	0.359 0.111	-0.409 -0.061	0.459 0.011	-0.509 0.039	-0.559 0.069	0.609 0.129	-0.659 0.159	-0.709 0.209	-0.759 0.259	-0.809 0.309	-0.859 0.359	-0.909 0.409	-0.959 0.459
-0.115 -0.135	-0.145 -0.105	-0.215 -0.055	0.235 0.005	0.315 0.045	-0.365 0.095	0.415 0.145	-0.415 0.195	-0.415 0.245	-0.415 0.295	-0.415 0.315	-0.415 0.335	-0.415 0.355	-0.415 0.375	-0.415 0.395	-0.415 0.415	-0.415 0.435
-0.195 -0.274	-0.245 -0.324	-0.295 -0.174	-0.345 -0.124	-0.395 -0.074	-0.445 -0.024	-0.495 0.026	-0.545 0.076	-0.595 0.126	-0.645 0.176	-0.695 0.226	-0.745 0.276	-0.795 0.326	-0.845 0.376	-0.895 0.426	-0.945 0.476	-0.995 0.526
0.316 0.213	0.265 0.243	0.216 0.313	0.166 0.363	0.116 0.413	0.066 0.463	0.016 0.513	-0.034 0.563	-0.084 0.613	-0.134 0.663	-0.184 0.713	-0.234 0.763	-0.284 0.813	-0.334 0.863	-0.384 0.913	-0.434 0.963	-0.484 1.013
0.250 0.119	0.200 0.166	0.150 0.219	0.100 0.269	0.050 0.319	0.000 0.369	-0.050 0.419	-0.100 0.469	-0.150 0.519	-0.200 0.569	-0.250 0.619	-0.300 0.669	-0.350 0.719	-0.400 0.769	-0.450 0.819	-0.500 0.869	-0.550 0.919
-0.363 -0.631	-0.613 -0.591	-0.463 -0.531	-0.513 -0.431	-0.563 -0.431	-0.613 -0.331	-0.663 -0.231	-0.713 -0.131	-0.763 -0.031	-0.813 0.069	-0.863 0.169	-0.913 0.269	-0.963 0.369	-1.013 0.469	-1.063 0.569	-1.113 0.669	-1.163 0.769
0.074 0.094	0.324 0.144	-0.032 0.134	-0.075 0.244	0.125 0.294	0.175 0.344	0.225 0.394	0.275 0.444	0.325 0.494	0.375 0.544	0.425 0.594	0.475 0.644	0.525 0.694	0.575 0.744	0.625 0.794	0.675 0.844	0.725 0.894
-0.068 0.019	-0.118 0.045	-0.168 0.110	-0.218 0.160	-0.268 0.210	-0.318 0.260	-0.368 0.310	-0.418 0.360	-0.468 0.410	-0.518 0.460	-0.568 0.510	-0.618 0.560	-0.668 0.610	-0.718 0.660	-0.768 0.710	-0.818 0.760	-0.868 0.810
0.396 0.167	0.245 0.217	0.296 0.267	0.346 0.317	0.396 0.367	0.446 0.417	0.496 0.467	0.546 0.517	0.596 0.567	0.646 0.617	0.696 0.667	0.746 0.717	0.796 0.767	0.846 0.817	0.896 0.867	0.946 0.917	0.996 0.967
-0.002 -0.071	-0.052 0.021	-0.102 0.079	-0.152 0.079	-0.202 0.129	-0.252 0.179	-0.302 0.229	-0.352 0.279	-0.402 0.329	-0.452 0.379	-0.502 0.429	-0.552 0.479	-0.602 0.529	-0.652 0.579	-0.702 0.629	-0.752 0.679	-0.802 0.729
-0.064 -0.337	-0.114 -0.287	-0.164 -0.237	-0.214 -0.167	-0.264 -0.137	-0.314 -0.087	-0.364 0.063	-0.414 0.113	-0.464 0.163	-0.514 0.213	-0.564 0.263	-0.614 0.313	-0.664 0.363	-0.714 0.413	-0.764 0.463	-0.814 0.513	-0.864 0.563
0.310 0.095	0.160 0.145	0.110 0.195	0.060 0.245	0.010 0.295	-0.040 0.345	-0.090 0.395	-0.140 0.445	-0.190 0.495	-0.240 0.545	-0.290 0.595	-0.340 0.645	-0.390 0.695	-0.440 0.745	-0.490 0.795	-0.540 0.845	-0.590 0.895
0.143 -0.037	0.093 0.013	0.043 0.063	-0.007 0.113	-0.057 0.163	-0.107 0.213	-0.157 0.263	-0.207 0.313	-0.257 0.363	-0.307 0.413	-0.357 0.463	-0.407 0.513	-0.457 0.563	-0.507 0.613	-0.557 0.663	-0.607 0.713	-0.657 0.763
-0.320 -0.529	-0.370 -0.579	-0.420 -0.529	-0.470 -0.479	-0.520 -0.429	-0.570 -0.379	-0.620 -0.329	-0.670 -0.279	-0.720 -0.229	-0.770 -0.179	-0.820 -0.129	-0.870 -0.079	-0.920 -0.029	-0.970 0.029	-1.020 0.079	-1.070 0.129	-1.120 0.179
0.185 0.002	0.135 0.052	0.085 0.102	0.035 0.152	0.005 0.202	-0.045 0.252	-0.095 0.302	-0.145 0.352	-0.195 0.402	-0.245 0.452	-0.295 0.502	-0.345 0.552	-0.395 0.602	-0.445 0.652	-0.495 0.702	-0.545 0.752	-0.595 0.802
0.321 0.009	0.271 0.059	0.221 0.109	0.171 0.159	0.121 0.209	0.071 0.259	0.021 0.309	-0.029 0.359	-0.079 0.409	-0.129 0.459	-0.179 0.509	-0.229 0.559	-0.279 0.609	-0.329 0.659	-0.379 0.709	-0.429 0.759	-0.479 0.809
0.174 0.049	0.124 0.139	0.074 0.159	0.024 0.239	-0.026 0.289	-0.076 0.339	-0.126 0.389	-0.176 0.439	-0.226 0.489	-0.276 0.539	-0.326 0.589	-0.376 0.639	-0.426 0.689	-0.476 0.739	-0.526 0.789	-0.576 0.839	-0.626 0.889
-0.234 -0.331	-0.284 -0.381	-0.334 -0.431	-0.384 -0.481	-0.434 -0.531	-0.484 -0.631	-0.534 -0.681	-0.584 -0.731	-0.634 -0.781	-0.684 -0.831	-0.734 -0.881	-0.784 -0.931	-0.834 -0.981	-0.884 -1.031	-0.934 -1.081	-0.984 -1.131	-1.034 -1.181

FIG 4(b)

00000 00000 00000

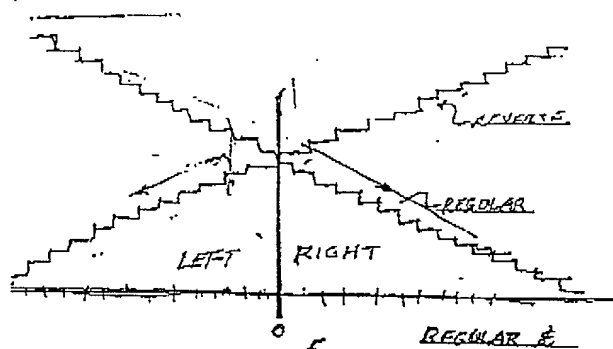


FIG 5 (a) REVERSE SCANS

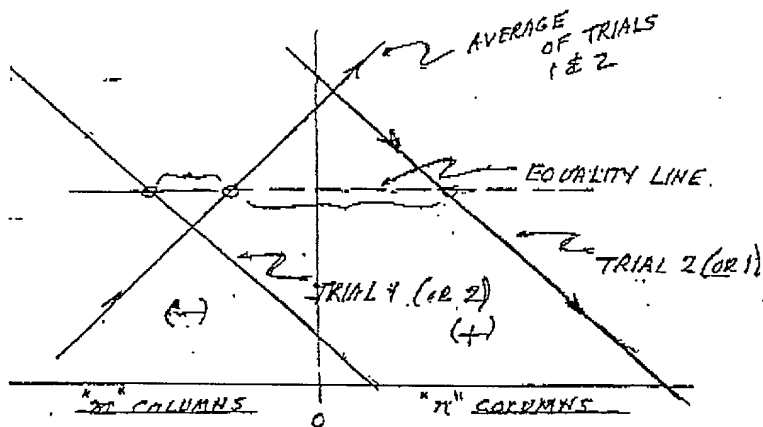


FIG 5 (b) COLUMN LOCATION

FIG 5 SCANNING "SENSE" REQUIREMENTS

I data ===		Average I values																*** Avg scanned in opposite sense ***	
Min 1A		-4 v	-3.5 v	-3 v	-2.5 v	-2 v	-1.5 v	-1 v	-0.5 v	0 v	0.5 v	1 v	1.5 v	2 v	2.5 v	3 v	3.5 v	4 v	
Avg		2.431	2.381	2.331	2.281	2.231	2.181	2.131	2.081	2.031	1.981	1.931	1.881	1.831	1.781	1.731	1.681	1.631	
20B	-0.041	0.672	0.722	0.772	0.822	0.872	0.922	0.972	1.022	1.072	1.122	1.172	1.222	1.272	1.322	1.372	1.422	1.472	
Avg		1.716	1.666	1.616	1.566	1.516	1.466	1.416	1.366	1.316	1.266	1.216	1.166	1.116	1.066	1.016	0.966	0.916	
21A	-0.052	0.064	0.114	0.164	0.214	0.264	0.314	0.364	0.414	0.464	0.514	0.564	0.614	0.664	0.714	0.764	0.814	0.864	
Avg		1.960	1.910	1.860	1.810	1.760	1.710	1.660	1.610	1.560	1.510	1.460	1.410	1.360	1.310	1.260	1.210	1.160	
22A	-0.060	0.220	0.270	0.320	0.370	0.420	0.470	0.520	0.570	0.620	0.670	0.720	0.770	0.820	0.870	0.920	0.970	1.020	
Avg		1.878	1.828	1.778	1.728	1.678	1.628	1.578	1.528	1.478	1.428	1.378	1.328	1.278	1.228	1.178	1.128	1.078	
23A	-0.022	0.101	0.151	0.201	0.251	0.301	0.351	0.401	0.451	0.501	0.551	0.601	0.651	0.701	0.751	0.801	0.851	0.901	
Avg		2.399	2.349	2.299	2.249	2.199	2.149	2.099	2.049	1.999	1.949	1.899	1.849	1.799	1.749	1.699	1.649	1.599	
24A	-0.002	0.568	0.618	0.668	0.718	0.768	0.818	0.868	0.918	0.968	1.018	1.068	1.118	1.168	1.218	1.268	1.318	1.368	
Avg		2.325	2.275	2.225	2.175	2.125	2.075	2.025	1.975	1.925	1.875	1.825	1.775	1.725	1.675	1.625	1.575	1.525	
25B	-0.032	0.493	0.543	0.593	0.643	0.693	0.743	0.793	0.843	0.893	0.943	0.993	1.043	1.093	1.143	1.193	1.243	1.293	
Avg		1.712	1.662	1.612	1.562	1.512	1.462	1.412	1.362	1.312	1.262	1.212	1.162	1.112	1.062	1.012	0.962	0.912	
26B	-0.169	0.257	0.307	0.357	0.407	0.457	0.507	0.557	0.607	0.657	0.707	0.757	0.807	0.857	0.907	0.957	1.007	1.057	
Avg		2.149	2.099	2.049	1.999	1.949	1.899	1.849	1.799	1.749	1.699	1.649	1.599	1.549	1.499	1.449	1.399	1.349	
27A	-0.120	0.458	0.508	0.558	0.608	0.658	0.708	0.758	0.808	0.858	0.908	0.958	1.008	1.058	1.108	1.158	1.208	1.258	
Avg		2.007	1.957	1.907	1.857	1.807	1.757	1.707	1.657	1.607	1.557	1.507	1.457	1.407	1.357	1.307	1.257	1.207	
28B	-0.178	0.385	0.435	0.485	0.535	0.585	0.635	0.685	0.735	0.785	0.835	0.885	0.935	0.985	1.035	1.085	1.135	1.185	
Avg		2.471	2.421	2.371	2.321	2.271	2.221	2.171	2.121	2.071	2.021	1.971	1.921	1.871	1.821	1.771	1.721	1.671	
29C	-0.129	0.542	0.592	0.642	0.692	0.742	0.792	0.842	0.892	0.942	0.992	1.042	1.092	1.142	1.192	1.242	1.292	1.342	
Avg		2.073	2.023	1.973	1.923	1.873	1.823	1.773	1.723	1.673	1.623	1.573	1.523	1.473	1.423	1.373	1.323	1.273	
30B	-0.032	0.304	0.354	0.404	0.454	0.504	0.554	0.604	0.654	0.704	0.754	0.804	0.854	0.904	0.954	1.004	1.054	1.104	
Avg		2.011	1.961	1.911	1.861	1.811	1.761	1.711	1.661	1.611	1.561	1.511	1.461	1.411	1.361	1.311	1.261	1.211	
31C	-0.174	0.037	0.087	0.137	0.187	0.237	0.287	0.337	0.387	0.437	0.487	0.537	0.587	0.637	0.687	0.737	0.787	0.837	
Avg		2.285	2.235	2.185	2.135	2.085	2.035	1.985	1.935	1.885	1.835	1.785	1.735	1.685	1.635	1.585	1.535	1.485	
32C	-0.015	0.470	0.520	0.570	0.620	0.670	0.720	0.770	0.820	0.870	0.920	0.970	1.020	1.070	1.120	1.170	1.220	1.270	
Avg		2.218	2.168	2.118	2.068	2.018	1.968	1.918	1.868	1.818	1.768	1.718	1.668	1.618	1.568	1.518	1.468	1.418	
33C	-0.080	0.338	0.388	0.438	0.488	0.538	0.588	0.638	0.688	0.738	0.788	0.838	0.888	0.938	0.988	1.038	1.088	1.138	
Avg		1.755	1.705	1.655	1.605	1.555	1.505	1.455	1.405	1.355	1.305	1.255	1.205	1.155	1.105	1.055	1.005	0.955	
34A	-0.209	0.255	0.305	0.355	0.405	0.455	0.505	0.555	0.605	0.655	0.705	0.755	0.805	0.855	0.905	0.955	1.005	1.055	
Avg		2.260	2.210	2.160	2.110	2.060	2.010	1.960	1.910	1.860	1.810	1.760	1.710	1.660	1.610	1.560	1.510	1.460	
35C	-0.083	0.377	0.427	0.477	0.527	0.577	0.627	0.677	0.727	0.777	0.827	0.877	0.927	0.977	1.027	1.077	1.127	1.177	
Avg		2.396	2.346	2.296	2.246	2.196	2.146	2.096	2.046	1.996	1.946	1.896	1.846	1.796	1.746	1.696	1.646	1.596	
36B	-0.212	0.384	0.434	0.484	0.534	0.584	0.634	0.684	0.734	0.784	0.834	0.884	0.934	0.984	1.034	1.084	1.134	1.184	
Avg		2.241	2.191	2.141	2.091	2.041	1.991	1.941	1.891	1.841	1.791	1.741	1.691	1.641	1.591	1.541	1.491	1.441	
37C	-0.015	0.463	0.513	0.563	0.613	0.663	0.713	0.763	0.813	0.863	0.913	0.963	1.013	1.063	1.113	1.163	1.213	1.263	
Avg		1.841	1.791	1.741	1.691	1.641	1.591	1.541	1.491	1.441	1.391	1.341	1.291	1.241	1.191	1.141	1.091	1.041	
38B	-0.003	0.616	0.666	0.716	0.766	0.816	0.866	0.916	0.966	1.016	1.066	1.116	1.166	1.216	1.266	1.316	1.366	1.416	

FILE 8(2)

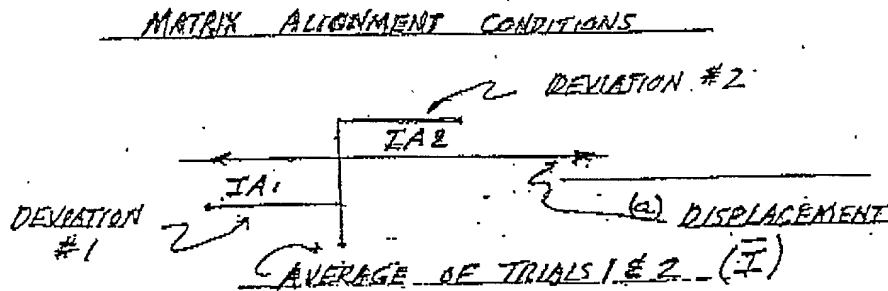
	I	II	III	IV	V	VI	VII	VIII	IX	X	XI	XII	XIII	XIV	XV	XVI	XVII	XVIII	XIX	XX	XXI	XXII	XXIII	XXIV	XXV	XXVI	XXVII	XXVIII	XXIX	XXX	XXXI	XXXII	XXXIII	XXXIV	XXXV	XXXVI	XXXVII	XXXVIII	XXXIX	XL	XL I	XL II	XL III	XL IV	XL V	XL VI	XL VII	XL VIII	XL IX	XL X	XL XI	XL XII	XL XIII	XL XIV	XL XV	XL XVI	XL XVII	XL XVIII	XL XIX	XL XX	XL XXI	XL XXII	XL XXIII	XL XXIV	XL XXV	XL XXVI	XL XXVII	XL XXVIII	XL XXIX	XL XXX	XL XXXI	XL XXXII	XL XXXIII	XL XXXIV	XL XXXV	XL XXXVI	XL XXXVII	XL XXXVIII	XL XXXIX	XL XL	XL XL I	XL XL II	XL XL III	XL XL IV	XL XL V	XL XL VI	XL XL VII	XL XL VIII	XL XL IX	XL XL X	XL XL XI	XL XL XII	XL XL XIII	XL XL XIV	XL XL XV	XL XL XVI	XL XL XVII	XL XL XVIII	XL XL XIX	XL XL XX	XL XL XXI	XL XL XXII	XL XL XXIII	XL XL XXIV	XL XL XXV	XL XL XXVI	XL XL XXVII	XL XL XXVIII	XL XL XXIX	XL XL XXX	XL XL XXXI	XL XL XXXII	XL XL XXXIII	XL XL XXXIV	XL XL XXXV	XL XL XXXVI	XL XL XXXVII	XL XL XXXVIII	XL XL XXXIX	XL XL XL	XL XL XL I	XL XL XL II	XL XL XL III	XL XL XL IV	XL XL XL V	XL XL XL VI	XL XL XL VII	XL XL XL VIII	XL XL XL IX	XL XL XL X	XL XL XL XI	XL XL XL XII	XL XL XL XIII	XL XL XL XIV	XL XL XL XV	XL XL XL XVI	XL XL XL XVII	XL XL XL XVIII	XL XL XL XIX	XL XL XL XX	XL XL XL XXI	XL XL XL XXII	XL XL XL XXIII	XL XL XL XXIV	XL XL XL XXV	XL XL XL XXVI	XL XL XL XXVII	XL XL XL XXVIII	XL XL XL XXIX	XL XL XL XXX	XL XL XL XXXI	XL XL XL XXXII	XL XL XL XXXIII	XL XL XL XXXIV	XL XL XL XXXV	XL XL XL XXXVI	XL XL XL XXXVII	XL XL XL XXXVIII	XL XL XL XXXIX	XL XL XL XL	XL XL XL XL I	XL XL XL XL II	XL XL XL XL III	XL XL XL XL IV	XL XL XL XL V	XL XL XL XL VI	XL XL XL XL VII	XL XL XL XL VIII	XL XL XL XL IX	XL XL XL XL X	XL XL XL XL XI	XL XL XL XL XII	XL XL XL XL XIII	XL XL XL XL XIV	XL XL XL XL XV	XL XL XL XL XVI	XL XL XL XL XVII	XL XL XL XL XVIII	XL XL XL XL XIX	XL XL XL XL XX	XL XL XL XL XXI	XL XL XL XL XXII	XL XL XL XL XXIII	XL XL XL XL XXIV	XL XL XL XL XXV	XL XL XL XL XXVI	XL XL XL XL XXVII	XL XL XL XL XXVIII	XL XL XL XL XXIX	XL XL XL XL XXX	XL XL XL XL XXXI	XL XL XL XL XXXII	XL XL XL XL XXXIII	XL XL XL XL XXXIV	XL XL XL XL XXXV	XL XL XL XL XXXVI	XL XL XL XL XXXVII	XL XL XL XL XXXVIII	XL XL XL XL XXXIX	XL XL XL XL XL	XL XL XL XL XL I	XL XL XL XL XL II	XL XL XL XL XL III	XL XL XL XL XL IV	XL XL XL XL XL V	XL XL XL XL XL VI	XL XL XL XL XL VII	XL XL XL XL XL VIII	XL XL XL XL XL IX	XL XL XL XL XL X	XL XL XL XL XL XI	XL XL XL XL XL XII	XL XL XL XL XL XIII	XL XL XL XL XL XIV	XL XL XL XL XL XV	XL XL XL XL XL XVI	XL XL XL XL XL XVII	XL XL XL XL XL XVIII	XL XL XL XL XL XIX	XL XL XL XL XL XX	XL XL XL XL XL XXI	XL XL XL XL XL XXII	XL XL XL XL XL XXIII	XL XL XL XL XL XXIV	XL XL XL XL XL XXV	XL XL XL XL XL XXVI	XL XL XL XL XL XXVII	XL XL XL XL XL XXVIII	XL XL XL XL XL XXIX	XL XL XL XL XL XXX	XL XL XL XL XL XXXI	XL XL XL XL XL XXXII	XL XL XL XL XL XXXIII	XL XL XL XL XL XXXIV	XL XL XL XL XL XXXV	XL XL XL XL XL XXXVI	XL XL XL XL XL XXXVII	XL XL XL XL XL XXXVIII	XL XL XL XL XL XXXIX	XL XL XL XL XL XL	XL XL XL XL XL XL I	XL XL XL XL XL XL II	XL XL XL XL XL XL III	XL XL XL XL XL XL IV	XL XL XL XL XL XL V	XL XL XL XL XL XL VI	XL XL XL XL XL XL VII	XL XL XL XL XL XL VIII	XL XL XL XL XL XL IX	XL XL XL XL XL XL X	XL XL XL XL XL XL XI	XL XL XL XL XL XL XII	XL XL XL XL XL XL XIII	XL XL XL XL XL XL XIV	XL XL XL XL XL XL XV	XL XL XL XL XL XL XVI	XL XL XL XL XL XL XVII	XL XL XL XL XL XL XVIII	XL XL XL XL XL XL XIX	XL XL XL XL XL XL XX	XL XL XL XL XL XL XXI	XL XL XL XL XL XL XXII	XL XL XL XL XL XL XXIII	XL XL XL XL XL XL XXIV	XL XL XL XL XL XL XXV	XL XL XL XL XL XL XXVI	XL XL XL XL XL XL XXVII	XL XL XL XL XL XL XXVIII	XL XL XL XL XL XL XXIX	XL XL XL XL XL XL XXX	XL XL XL XL XL XL XXXI	XL XL XL XL XL XL XXXII	XL XL XL XL XL XL XXXIII	XL XL XL XL XL XL XXXIV	XL XL XL XL XL XL XXXV	XL XL XL XL XL XL XXXVI	XL XL XL XL XL XL XXXVII	XL XL XL XL XL XL XXXVIII	XL XL XL XL XL XL XXXIX	XL XL XL XL XL XL XL	XL XL XL XL XL XL XL I	XL XL XL XL XL XL XL II	XL XL XL XL XL XL XL III	XL XL XL XL XL XL XL IV	XL XL XL XL XL XL XL V	XL XL XL XL XL XL XL VI	XL XL XL XL XL XL XL VII	XL XL XL XL XL XL XL VIII	XL XL XL XL XL XL XL IX	XL XL XL XL XL XL XL X	XL XL XL XL XL XL XL XI	XL XL XL XL XL XL XL XII	XL XL XL XL XL XL XL XIII	XL XL XL XL XL XL XL XIV	XL XL XL XL XL XL XL XV	XL XL XL XL XL XL XL XVI	XL XL XL XL XL XL XL XVII	XL XL XL XL XL XL XL XVIII	XL XL XL XL XL XL XL XIX	XL XL XL XL XL XL XL XX	XL XL XL XL XL XL XL XXI	XL XL XL XL XL XL XL XXII	XL XL XL XL XL XL XL XXIII	XL XL XL XL XL XL XL XXIV	XL XL XL XL XL XL XL XXV	XL XL XL XL XL XL XL XXVI	XL XL XL XL XL XL XL XXVII	XL XL XL XL XL XL XL XXVIII	XL XL XL XL XL XL XL XXIX	XL XL XL XL XL XL XL XXX	XL XL XL XL XL XL XL XXXI	XL XL XL XL XL XL XL XXXII	XL XL XL XL XL XL XL XXXIII	XL XL XL XL XL XL XL XXXIV	XL XL XL XL XL XL XL XXXV	XL XL XL XL XL XL XL XXXVI	XL XL XL XL XL XL XL XXXVII	XL XL XL XL XL XL XL XXXVIII	XL XL XL XL XL XL XL XXXIX	XL XL XL XL XL XL XL XL	XL XL XL XL XL XL XL XL I	XL XL XL XL XL XL XL XL II	XL XL XL XL XL XL XL XL III	XL XL XL XL XL XL XL XL IV	XL XL XL XL XL XL XL XL V	XL XL XL XL XL XL XL XL VI	XL XL XL XL XL XL XL XL VII	XL XL XL XL XL XL XL XL VIII	XL XL XL XL XL XL XL XL IX	XL XL XL XL XL XL XL XL X	XL XL XL XL XL XL XL XL XI	XL XL XL XL XL XL XL XL XII	XL XL XL XL XL XL XL XL XIII	XL XL XL XL XL XL XL XL XIV	XL XL XL XL XL XL XL XL XV	XL XL XL XL XL XL XL XL XVI	XL XL XL XL XL XL XL XL XVII	XL XL XL XL XL XL XL XL XVIII	XL XL XL XL XL XL XL XL XIX	XL XL XL XL XL XL XL XL XX	XL XL XL XL XL XL XL XL XXI	XL XL XL XL XL XL XL XL XXII	XL XL XL XL XL XL XL XL XXIII	XL XL XL XL XL XL XL XL XXIV	XL XL XL XL XL XL XL XL XXV	XL XL XL XL XL XL XL XL XXVI	XL XL XL XL XL XL XL XL XXVII	XL XL XL XL XL XL XL XL XXVIII	XL XL XL XL XL XL XL XL XXIX	XL XL XL XL XL XL XL XL XXX	XL XL XL XL XL XL XL XL XXXI	XL XL XL XL XL XL XL XL XXXII	XL XL XL XL XL XL XL XL XXXIII	XL XL XL XL XL XL XL XL XXXIV	XL XL XL XL XL XL XL XL XXXV	XL XL XL XL XL XL XL XL XXXVI	XL XL XL XL XL XL XL XL XXXVII	XL XL XL XL XL XL XL XL XXXVIII	XL XL XL XL XL XL XL XL XXXIX	XL XL XL XL XL XL XL XL XL	XL XL XL XL XL XL XL XL XL I	XL XL XL XL XL XL XL XL XL II	XL XL XL XL XL XL XL XL XL III	XL XL XL XL XL XL XL XL XL IV	XL XL XL XL XL XL XL XL XL V	XL XL XL XL XL XL XL XL XL VI	XL XL XL XL XL XL XL XL XL VII	XL XL XL XL XL XL XL XL XL VIII	XL XL XL XL XL XL XL XL XL IX	XL XL XL XL XL XL XL XL XL X	XL XL XL XL XL XL XL XL XL XI	XL XL XL XL XL XL XL XL XL XII	XL XL XL XL XL XL XL XL XL XIII	XL XL XL XL XL XL XL XL XL XIV	XL XL XL XL XL XL XL XL XL XV	XL XL XL XL XL XL XL XL XL XVI	XL XL XL XL XL XL XL XL XL XVII	XL XL XL XL XL XL XL XL XL XVIII	XL XL XL XL XL XL XL XL XL XIX	XL XL XL XL XL XL XL XL XL XX	XL XL XL XL XL XL XL XL XL XXI	XL XL XL XL XL XL XL XL XL XXII	XL XL XL XL XL XL XL XL XL XXIII	XL XL XL XL XL XL XL XL XL XXIV	XL XL XL XL XL XL XL XL XL XXV	XL XL XL XL XL XL XL XL XL XXVI	XL XL XL XL XL XL XL XL XL XXVII	XL XL XL XL XL XL XL XL XL XXVIII	XL XL XL XL XL XL XL XL XL XXIX	XL XL XL XL XL XL XL XL XL XXX	XL XL XL XL XL XL XL XL XL XXXI	XL XL XL XL XL XL XL XL XL XXXII	XL XL XL XL XL XL XL XL XL XXXIII	XL XL XL XL XL XL XL XL XL XXXIV	XL XL XL XL XL XL XL XL XL XXXV	XL XL XL XL XL XL XL XL XL XXXVI	XL XL XL XL XL XL XL XL XL XXXVII	XL XL XL XL XL XL XL XL XL XXXVIII	XL XL XL XL XL XL XL XL XL XXXIX	XL XL XL XL XL XL XL XL XL XL	XL XL XL XL XL XL XL XL XL XL I	XL XL XL XL XL XL XL XL XL XL II	XL XL XL XL XL XL XL XL XL XL III	XL XL XL XL XL XL XL XL XL XL IV	XL XL XL XL XL XL XL XL XL XL V	XL XL XL XL XL XL XL XL XL XL VI	XL XL XL XL XL XL XL XL XL XL VII	XL XL XL XL XL XL XL XL XL XL VIII	XL XL XL XL XL XL XL XL XL XL IX	XL XL XL XL XL XL XL XL XL XL X	XL XL XL XL XL XL XL XL XL XL XI	XL XL XL XL XL XL XL XL XL XL XII	XL XL XL XL XL XL XL XL XL XL XIII	XL XL XL XL XL XL XL XL XL XL XIV	XL XL XL XL XL XL XL XL XL XL XV	XL XL XL XL XL XL XL XL XL XL XVI	XL XL XL XL XL XL XL XL XL XL XVII	XL XL XL XL XL XL XL XL XL XL XVIII	XL XL XL XL XL XL XL XL XL XL XIX	XL XL XL XL XL XL XL XL XL XL XX	XL XL XL XL XL XL XL XL XL XL XXI	XL XL XL XL XL XL XL XL XL XL XXII	XL XL XL XL XL XL XL XL XL XL XXIII	XL XL XL XL XL XL XL XL XL XL XXIV	XL XL XL XL XL XL XL XL XL XL XXV	XL XL XL XL XL XL XL XL XL XL XXVI	XL XL XL XL XL XL XL XL XL XL XXVII	XL XL XL XL XL XL XL XL XL XL XXVIII	XL XL XL XL XL XL XL XL XL XL XXIX	XL XL XL XL XL XL XL XL XL XL XXX	XL XL XL XL XL XL XL XL XL XL XXXI	XL XL XL XL XL XL XL XL XL XL XXXII	XL XL XL XL XL XL XL XL XL XL XXXIII	XL XL XL XL XL XL XL XL XL XL XXXIV	XL XL XL XL XL XL XL XL XL XL XXXV	XL XL XL XL XL XL XL XL XL XL XXXVI	XL XL XL XL XL XL XL XL XL XL XXXVII	XL XL XL XL XL XL XL XL XL XL XXXVIII	XL XL XL XL XL XL XL XL XL XL XXXIX	XL XL XL XL XL XL XL XL XL XL XL	XL XL XL XL XL XL XL XL XL XL XL I	XL XL XL XL XL XL XL XL XL XL XL II	XL XL XL XL XL XL XL XL XL XL XL III	XL XL XL XL XL XL XL XL XL XL XL IV	XL XL XL XL XL XL XL XL XL XL XL V	XL XL XL XL XL XL XL XL XL XL XL VI	XL XL XL XL XL XL XL XL XL XL XL VII	XL XL XL XL XL XL XL XL XL XL XL VIII	XL XL XL XL XL XL XL XL XL XL XL IX	XL XL XL XL XL XL XL XL XL XL XL X	XL XL XL XL XL XL XL XL XL XL XL XI	XL XL XL XL XL XL XL XL XL XL XL XII	XL XL XL XL XL XL XL XL XL XL XL XIII	XL XL XL XL XL XL XL XL XL XL XL XIV	XL XL XL XL XL XL XL XL XL XL XL XV	XL XL XL XL XL XL XL XL XL XL XL XVI	XL XL XL XL XL XL XL XL XL XL XL XVII	XL XL XL XL XL XL XL XL XL XL XL XVIII	XL XL XL XL XL XL XL XL XL XL XL XIX	XL XL XL XL XL XL XL XL XL XL XL XX	XL XL XL XL XL XL XL XL XL XL XL XXI	XL XL XL XL XL XL XL XL XL XL XL XXII	XL XL XL XL XL XL XL XL XL XL XL XXIII	XL XL XL XL XL XL XL XL XL XL XL XXIV	XL XL XL XL XL XL XL XL XL XL XL XXV	XL XL XL XL XL XL XL XL XL XL XL XXVI	XL XL XL XL XL XL XL XL XL XL XL XXVII	XL XL XL XL XL XL XL XL XL XL XL XXVIII	XL XL XL XL XL XL XL XL XL XL XL XXIX	XL XL XL XL XL XL XL XL XL XL XL XXX	XL XL XL XL XL XL XL XL XL XL XL XXXI	XL XL XL XL XL XL XL XL XL XL XL XXXII	XL XL XL XL XL XL XL XL XL XL XL XXXIII	XL XL XL XL XL XL XL XL XL XL XL XXXIV	XL XL XL XL XL XL XL XL XL XL XL XXXV	XL XL XL XL XL XL XL XL XL XL XL XXXVI	XL XL XL XL XL XL XL XL XL XL XL XXXVII	XL XL XL XL XL XL XL XL XL XL XL XXXVIII	XL XL XL XL XL XL XL XL XL XL XL XXXIX	XL XL XL XL XL XL XL XL XL XL XL XL	XL XL XL XL XL XL XL XL XL XL XL XL I	XL XL XL XL XL XL XL XL XL XL XL XL II	XL XL XL XL XL XL XL XL XL XL XL XL III	XL XL XL XL XL XL XL XL XL XL XL XL IV	XL XL XL XL XL XL XL XL XL XL XL XL V	XL XL XL XL XL XL XL XL XL XL XL XL VI	XL XL XL XL XL XL XL XL XL XL XL XL VII	XL XL XL XL XL XL XL XL XL XL XL XL VIII	XL XL XL XL XL XL XL XL XL XL XL XL IX	XL XL XL XL XL XL XL XL XL XL XL XL X	XL XL XL XL XL XL XL XL XL XL XL XL XI	XL XL XL XL XL XL XL XL XL XL XL XL XII	XL XL XL XL XL XL XL XL XL XL XL XL XIII	XL XL XL XL XL XL XL XL XL XL XL XL XIV	XL XL XL XL XL XL XL XL XL XL XL XL XV	XL XL XL XL XL XL XL XL XL XL XL XL XVI	XL XL XL XL XL XL XL XL XL XL XL XL XVII	XL XL XL XL XL XL XL XL XL XL XL XL XVIII	XL XL XL XL XL XL XL XL XL XL XL XL XIX	XL XL XL XL XL XL XL XL XL XL XL XL XX	XL XL XL XL XL XL XL XL XL XL XL XL XXI	XL XL XL XL XL XL XL XL XL XL XL XL XXII	XL XL XL XL XL XL XL XL XL XL XL XL XXIII	XL XL XL XL XL XL XL XL XL XL XL XL XXIV	XL XL XL XL XL XL XL XL XL XL XL XL XXV	XL XL XL XL XL XL XL XL XL XL XL XL XXVI	XL XL XL XL XL XL XL XL XL XL XL XL XXVII	XL XL XL XL XL XL XL XL XL XL XL XL XXVIII	XL XL XL XL XL XL XL XL XL XL XL XL XXIX	XL XL XL XL XL XL XL XL XL XL XL XL XXX	XL XL XL XL XL XL XL XL XL XL XL XL XXXI	XL XL XL XL XL XL XL XL XL XL XL XL XXXII	XL XL XL XL XL XL XL XL XL XL XL XL XXXIII	XL XL XL XL XL XL XL XL XL XL XL XL XXXIV	XL XL XL XL XL XL XL XL XL XL XL XL XXXV	XL XL XL XL XL XL XL XL XL XL XL XL XXXVI	XL XL XL XL XL XL XL XL XL XL XL XL XXXVII	XL XL XL XL XL XL XL XL XL XL XL XL XXXVIII	XL XL XL XL XL XL XL XL XL XL XL XL XXXIX	XL XL XL XL XL XL XL XL XL XL XL XL XL	XL XL XL XL XL XL XL XL XL XL XL XL XL I	XL XL XL XL XL XL XL XL XL XL XL XL XL II	XL XL XL XL XL XL XL XL XL XL XL XL XL III	XL XL XL XL XL XL XL XL XL XL XL XL XL IV	XL XL XL XL XL XL XL XL XL XL XL XL XL V	XL XL XL XL XL XL XL XL XL XL XL XL XL VI	XL XL XL XL XL 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XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXXIII	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXXIV	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXXV	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXXVI	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXXVII	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXXVIII	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXXIX	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL I	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL II	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL III	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL IV	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL V	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL VI	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL VII	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL VIII	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL IX	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL X	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XI	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XII	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XIII	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XIV	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XV	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XVI	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XVII	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XVIII	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XIX	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XX	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXI	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXII	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXIII	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXIV	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXV	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXVI	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXVII	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXVIII	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXIX	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXX	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXXI	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXXII	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXXIII	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXXIV	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXXV	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXXVI	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXXVII	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXXVIII	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXXIX	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL I	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL II	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL III	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL IV	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL V	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL VI	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL VII	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL VIII	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL IX	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL X	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XI	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XII	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XIII	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XIV	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XV	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XVI	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XVII	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XVIII	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XIX	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XX	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXI	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXII	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXIII	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXIV	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXV	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXVI	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXVII	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXVIII	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXIX	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXX	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXXI	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXXII	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXXIII	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXXIV	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXXV	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXXVI	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXXVII	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXXVIII	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXXIX	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL I	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL II	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL III	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL IV	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL V	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL VI	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL VII	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL VIII	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL IX	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL X	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XI	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XII	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XIII	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XIV	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XV	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XVI	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XVII	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XVIII	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XIX	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XX	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXI	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXII	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXIII	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXIV	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXV	XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XL XXVI	
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FIG 7 TOPOLOGICAL CHANGE SENSOR (IN EQUILIBRIUM)

FIGURE 8 TABLE OF INITIAL CONDITIONS & INSTRUCTIONS

Initial Conditions - (Iteration Zero)

USE FIGURE 7 AS A TYPOLOGICAL NUMBER ARRAY, WHICH HAS BEEN PLACED IN EQUILIBRIUM BY THE COLUMNS SHIFTING FUNCTIONING OF THE DEVIATIONS SHOWN BELOW (SO AS TO MAKE IT A "CHANGE SENSOR").



NOTE THAT: AVERAGE $I = I_{\text{signal}} + I_{\text{average noise}}$

ROW OF MINIMUM ABSOLUTE DEVIATION: $I_{\text{signal}} = I_{\text{noise}}$ closest to A_v noise

AMOUNT OF DEVIATION = $|IA|$ of the \pm polarity

OF EQUIVALENT COLUMN SHIFT = $|IA| \div \text{COLUMN SPACING}$

To start the iterative process note the entry of the signal-plus-noise in the zero column as the starting reference.

Obtain a numerical match of the entry value in the particular column in the second row which matches that in the 0 column. The column match will occur in either the right or left section.

NOTE: ENTRIES ARE ENTERED IN THE "AVERAGE ROW" COLUMN IN A SEQUENCE OPPOSITE THAT OF THE OTHER ROW

```

graph TD
    Start([LOCATION OF COLUMNS MATCH]) --> D1{LEFT RIGHT TCS}
    D1 -- LEFT --> D2{CHANGED SIDES?}
    D1 -- RIGHT --> D3{CHANGED SIDES?}
    D2 -- YES --> B1[1/2]
    D2 -- NO --> D4{CLOSER FARTHER TO 0?}
    D3 -- YES --> B2[1/2]
    D3 -- NO --> D5{CLOSER FARTHER TO 0?}
    B1 --> C1[CONTINUE NEW POLARITY]
    B2 --> C2[SAME POLARITY]
    D4 -- CLOSER --> B3[1/2?]
    D4 -- FARTHER --> B4[3/2]
    D5 -- CLOSER --> B5[1/2?]
    D5 -- FARTHER --> B6[3/2]
    B3 --> C3[CHANGE TO NEW POLARITY]
    B4 --> C4[CHANGE TO NEW POLARITY]
    B5 --> C3
    B6 --> C4
    C1 --> End([NEXT PROBE VALUE  
(MAGNITUDE & POLARITY)  
CHOOSE ONLY ONE!])
    C2 --> End
    C3 --> End
    C4 --> End
    End -- CHOICE --> End
  
```

FIG 9 SELECTION LOGIC FOR NEXT ITERATIVE PROBE

ITERATIVE INPUTS (PROBES)

ITERATIVE SELECTIVE DECISIONS

1 2 3 4 N-2 N-1 N

1 2 3 4 N-2 N-1 N ALGEBRAIC SUM OF VALUES

ITERATIVE PROBE VALUES + 1

CONSEQUENCES OF PROBE ITERATIONS

= NOISE ESTIMATE

ITERATIVE PROCESS

FIG 10. ITERATIVE PROCESS

Figure 1 consists of 12 line drawings of a chick embryo at different stages of development, arranged vertically and labeled 1 through 12. The drawings show the progression from a single cell (1) to a fully formed chick with a beak and legs (12). The stages are: 1. Fertilized egg, 2. Two-cell stage, 3. Four-cell stage, 4. Morula stage, 5. Gastrula stage, 6. Early neurulation, 7. Late neurulation, 8. Early hatching, 9. Late hatching, 10. Hatched chick, 11. Hatched chick with yolk sac, 12. Hatched chick with yolk sac and beak.

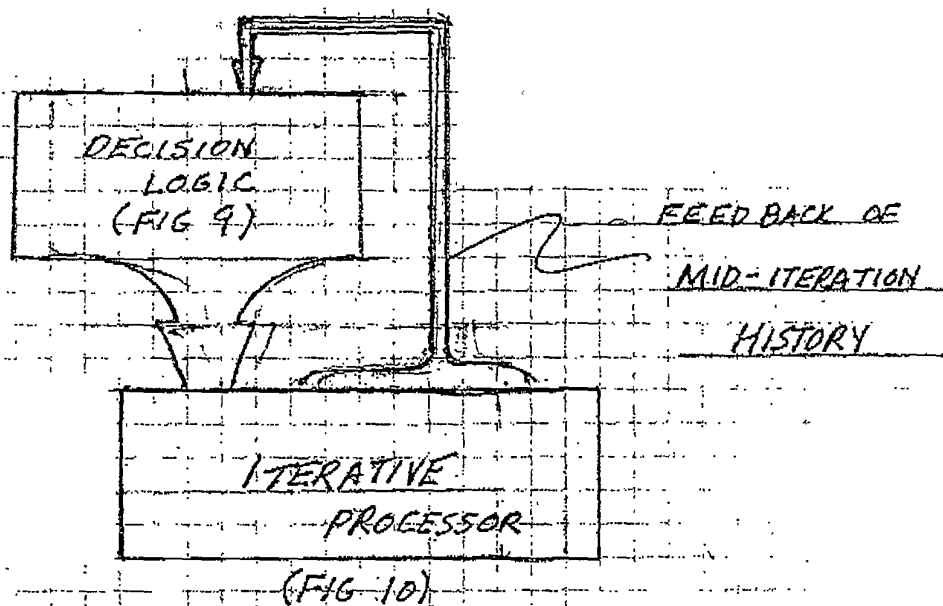


FIG 11 AUGMENTATION OF SELECTION LOGIC

result I data

Trial Group	Ordy	Noise Avg	New Noise Model					Equival Noise Added	Lact Noise Avg	Kallu Noise Avg
			1	2	3	4	5			
205	1	0.1481	0.0588	-0.1814	0.0622	-0.0224	0.0081	-0.1733	-0.0222	5.9
205	2	0.5428	0.3662	0.1105	-0.1856	-0.0006	0.0531	-0.0601	0.0222	4.2
205	3	0.6213	0.5902	0.2502	0.0002	-0.1249	-0.0023	-0.0524	-0.0511	20.0
206		-0.2508	-0.0508	0.1772	-0.2554	0.0542	0.0117	0.2313	-0.0176	12.0
206		0.1813	0.1442	0.1558	-0.1142	0.0108	-0.017	0.2017	-0.0205	4.3
206	3	0.4060	-0.3125	-0.0505	0.1822	0.0583	-0.0040	0.4332	0.0272	14.9
207	1	-0.2893	0.0300	0.2200	-0.0500	0.0930	0.0000	0.2906	0.0013	226.5
207	2	-0.0591	0.1266	-0.1232	0.1266	0.0018	-0.0070	0.0270	-0.0245	2.0
207	3	0.8016	0.7704	0.5404	0.2704	0.1654	0.1324	-0.7300	0.0716	11.2
208	1	-0.3264	-0.1353	0.1243	-0.1353	-0.0605	0.0605	0.0370	0.0306	10.0
208		-0.5892	-0.4820	-0.2026	0.0472	-0.0378	-0.0133	0.0052	0.0160	50.9
208		-0.5162	-0.3509	-0.1009	0.1471	0.0241	-0.0364	0.0099	-0.0071	72.4
209		-0.3328	-0.2313	0.0405	-0.2915	-0.1065	-0.0440	0.3200	-0.0128	26.1
209		0.7863	0.6288	0.3760	0.1246	0.0030	-0.0509	-0.0400	-0.0277	20.3
209		-0.3126	-0.1995	0.0504	-0.1995	-0.0746	-0.0121	0.3355	0.0192	16.4
210		-0.4253	-0.2432	0.0000	-0.2432	-0.1182	-0.0557	0.4107	-0.0241	17.0
210		-0.1066	0.1332	0.1332	0.0062	-0.0543	0.0636	-0.0230	0.0230	4.0
210		0.2597	0.0637	-0.2543	0.0637	-0.0346	-0.0346	-0.2552	-0.0505	48.7
211		-0.1477	-0.0020	0.1286	-0.0020	0.0033	0.0405	0.2323	0.0075	26.7
211		-0.2273	-0.2146	0.0300	-0.2146	-0.0665	-0.0263	0.2323	0.0047	76.0
211		0.0772	0.2340	0.2490	0.0340	-0.0340	0.0341	-0.0777	0.0005	820.7
212	1	0.1140	-0.2223	0.017	-0.2223	-0.1673	-0.0040	-0.2223	-0.0130	8.4
212		0.3209	0.2303	0.0034	-0.2477	-0.1247	-0.0622	-0.0016	-0.0009	10.4
212		0.2595	0.2157	-0.0341	0.2157	0.0746	-0.2224	-0.2224	-0.0027	70.1
213		0.4217	0.2641	-0.0277	0.2641	0.0071	0.0071	-0.1133	0.0034	120.0
213		-0.6357	0.3012	-0.0012	0.1700	0.0738	0.0112	0.2137	-0.0177	26.7
213		-0.2943	-0.2743	-0.0248	0.2222	0.1002	0.0377	0.3008	0.0005	45.0
214		-0.6983	-0.5029	-0.2527	-0.0624	0.1221	0.0576	0.7267	0.0030	44.0
214		0.7664	0.7016	0.4316	0.2016	0.0766	0.0141	-0.7800	-0.0171	14.7
214		0.3609	0.2261	-0.0219	0.2261	0.1081	0.0046	-0.3510	0.0043	88.7
215		-0.5994	-0.3920	-0.1420	0.1080	-0.0170	0.0455	0.1331	0.0146	44.1
215		-0.6416	-0.6115	-0.3635	-0.1115	0.0081	-0.0544	0.1187	-0.0231	27.6
215		-0.2020	-0.0166	0.2334	-0.0266	0.1080	0.0435	0.2100	0.0140	15.0
216		0.2267	-0.0609	0.2471	-0.0503	0.1241	0.0616	-0.1964	0.0305	7.5
216		-0.7664	-0.7607	-0.5107	-0.2607	-0.1357	-0.0732	0.1450	-0.0414	18.8
216	3	-0.3518	-0.0974	0.1500	-0.0594	0.0256	-0.0364	0.3422	-0.0057	81.0
217		-0.3160	-0.0968	0.1532	-0.0968	0.0262	-0.0343	0.3198	-0.0031	103.9
217		0.3848	0.3126	0.0626	-0.1874	-0.0624	0.0091	-0.4100	0.0312	12.3
217		0.3492	0.2517	0.0017	-0.2483	-0.1233	-0.0605	-0.3788	-0.0295	11.8
218		0.2194	0.0294	-0.2246	0.0294	-0.0746	-0.0371	0.2253	-0.0057	37.2
218		-0.6434	-0.5992	-0.3498	-0.0548	0.0253	-0.0378	0.0375	-0.0061	106.0
218		0.2516	0.1355	-0.1145	0.1355	0.0105	-0.0322	-0.2724	-0.0207	12.1
219		-0.6197	-0.3113	-0.2613	-0.0143	0.1137	0.0512	0.4376	0.0200	41.1
219		-0.1859	0.0141	-0.2654	0.0141	-0.1109	-0.0404	0.1666	-0.0172	10.6
219		-0.2779	-0.1231	0.1264	-0.1231	0.0019	-0.0000	0.2460	-0.0294	3.5
220		-0.2206	-0.0730	0.1744	-0.0730	0.0081	-0.0141	0.2472	-0.0121	12.1
220		-0.2723	-0.1005	0.0791	-0.1005	-0.0471	-0.0140	0.2582	-0.0140	22.0
220		0.0834	-0.0404	0.2072	-0.0404	0.1000	0.0121	0.0770	-0.0071	9.4
221		0.3421	-0.2118	0.0380	-0.2118	-0.0000	-0.0000	0.3793	0.0000	50.6
221		0.8987	0.8632	0.6432	0.2632	0.2400	0.0771	0.0433	0.0000	13.7
221		-0.3328	-0.0070	-0.0670	-0.0670	-0.0000	-0.0000	0.0000	0.0000	3.0

ORIGINAL
NOISE

RESULT OF EACH OF 1ST
(OF SIX ITERATIONS)

RESIDUAL VOLTAGE
NOISE RATIO

THIS
COLUMN
YIELDS
"ESTIMATE"
NOISE
(SUM OF VALUES)
ADDED

FIG 12 (a)

RAMMUT Q data

Trial/ Group	Orig Noise Avg	New Noise Average					Equip Voltage Added	Last Noise Avg	Ratio Orig to Last
		1	2	3	4	5			
205 1	0.4440	0.3979	0.1479	-0.1030	0.0220	-0.0409	-0.4582	-0.0094	48.1
205 2	0.1428	0.0077	-0.2423	0.0077	-0.1173	-0.0546	-0.2163	-0.0235	6.2
205 3	0.2307	0.0307	-0.2193	0.0307	-0.0943	-0.0318	-0.2313	-0.0008	292.9
206 1	0.6647	0.6647	0.3149	0.0649	-0.0601	0.0024	-0.6955	-0.0289	23.1
206 2	-0.0359	0.1153	-0.134	0.1153	-0.0097	0.0528	0.1174	0.0215	4.5
206 3	0.0218	-0.2543	-0.0065	0.2435	0.1185	0.0360	0.0030	0.0248	0.9
207 1	0.7412	0.7194	0.4694	0.2194	0.0944	0.0319	-0.7406	0.0006	1181.1
207 2	-0.2973	-0.2522	-0.0022	0.2478	0.1228	0.0603	0.3263	0.0290	10.2
207 3	0.3831	-0.0517	0.1983	-0.0517	0.0733	0.0108	-0.4024	-0.0205	18.7
208 1	0.2199	0.1728	-0.0772	0.1728	0.0478	-0.0147	-0.2033	0.0166	13.3
208 2	0.4198	0.3966	0.1464	-0.1034	0.0216	-0.0409	-0.4295	-0.0097	43.4
208 3	-0.1523	-0.0900	0.1600	-0.0900	0.0350	-0.0275	0.1561	0.0038	40.1
209 1	-0.3053	-0.2665	-0.0185	0.2315	0.1065	0.0440	0.3161	0.0127	23.8
209 2	-0.0800	0.0528	-0.1972	0.0528	-0.0722	-0.0097	0.1024	0.0214	3.7
209 3	-0.0148	0.1385	-0.1115	0.1385	0.0135	-0.0430	-0.0029	-0.0177	0.3
210 1	0.2507	0.1407	-0.0693	0.1607	0.0357	-0.0268	-0.2462	0.0044	56.8
210 2	0.2427	0.2049	-0.0451	0.2049	0.0799	0.0174	-0.2564	-0.0139	17.5
210 3	0.0941	-0.0741	0.1739	-0.0741	0.0489	-0.0134	-0.0784	0.0177	5.4
211 1	0.2297	0.2232	-0.0248	0.2232	0.0902	0.0357	-0.2325	0.0044	53.5
211 2	0.4845	0.2554	0.0034	-0.2444	-0.1216	-0.0591	-0.5143	-0.0278	17.5
211 3	-0.7412	-0.7029	-0.4554	-0.2039	-0.0728	-0.0164	0.7560	0.0146	50.1
212 1	0.5285	0.3926	0.1426	-0.1074	0.0176	-0.0449	-0.5421	-0.0136	38.2
212 2	0.1817	0.0820	-0.1479	0.0820	-0.0420	0.0204	-0.1925	-0.0107	16.9
212 3	-0.0208	0.1426	-0.1086	0.1420	0.0170	-0.0455	0.0646	-0.0142	1.5
213 1	-0.2570	-0.1652	0.0848	-0.1652	-0.0402	0.0223	0.2480	-0.0090	28.7
213 2	-0.0064	0.0210	-0.2190	0.0310	-0.0940	-0.0815	0.0062	-0.0003	24.3
213 3	-0.5094	-0.2200	-0.0700	0.1600	0.0550	-0.0075	0.5333	0.0237	21.5
214 1	-0.0246	0.1703	-0.0797	0.1703	0.0453	-0.0172	0.0337	0.0141	1.8
214 2	-0.1595	-0.0942	0.1506	-0.0942	0.0328	-0.0226	0.1620	0.0025	62.8
214 3	0.1216	-0.0494	0.2004	-0.0494	0.0754	0.0131	-0.1398	-0.0181	6.7
215 1	-0.3403	-0.0218	0.2287	-0.0213	0.1037	0.0412	0.3502	0.0099	54.3
215 2	-0.1557	-0.0242	0.2257	-0.0243	0.1007	0.0382	0.1627	0.0069	22.4
215 3	-0.5943	-0.3637	-0.0537	0.1963	0.0713	0.0086	0.5718	-0.0225	26.5
216 1	0.1584	0.0262	-0.2218	0.0262	-0.0968	-0.0343	-0.1614	-0.0030	52.0
216 2	0.3981	0.3794	0.1274	-0.1266	0.0044	-0.0581	-0.4250	-0.0268	14.0
216 3	0.1159	-0.0841	0.1659	-0.0841	-0.0409	-0.0216	-0.1063	0.0097	12.0
217 1	0.4437	0.2497	-0.0003	0.2497	0.1247	0.0622	-0.4188	0.0309	14.5
217 2	0.5273	0.2169	-0.0931	0.2169	0.0919	-0.0294	-0.5292	-0.0019	278.7
217 3	0.1066	-0.0700	0.1600	-0.0700	0.0550	-0.0075	-0.0829	0.0238	4.5
218 1	-0.4485	-0.2822	-0.0322	0.2178	0.0928	0.0303	0.4475	-0.0010	453.7
218 2	0.0383	-0.1447	0.1052	-0.1447	-0.0197	0.0428	-0.0867	0.0115	8.5
218 3	0.0171	-0.1190	0.1210	-0.1190	0.0660	-0.0545	-0.0423	-0.0252	0.7
219 1	0.0508	-0.1111	0.1387	-0.1111	0.0139	-0.0486	-0.0681	-0.0173	2.9
219 2	0.2668	0.0668	-0.1814	0.0668	-0.0582	0.0043	-0.2938	-0.0270	9.9
219 3	-0.2792	-0.1891	0.0607	-0.1891	-0.0441	-0.0016	0.3088	0.0296	9.4
220 1	0.6507	0.4095	0.3593	0.1035	-0.0155	0.0470	-0.6149	0.0158	41.2
220 2	0.6336	0.2617	0.1117	-0.1383	-0.0132	0.0492	-0.6157	0.0179	35.4
220 3	-0.1340	0.1748	-0.0794	0.1748	0.0498	-0.0127	0.1545	0.0185	7.2
221 1	-0.3741	-0.1141	0.1257	-0.1141	0.0109	-0.0515	0.2938	-0.0204	15.4
221 2	-0.0550	0.1447	-0.1053	0.1447	0.0197	-0.0428	0.0235	-0.0114	3.0
221 3	0.1025	-0.1267	0.1147	-0.1267	-0.0117	0.0500	-0.0979	0.0199	5.3

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